# CHAPTER 17 EQUILIBRIUM: THE EXTENT OF CHEMICAL REACTIONS

# FOLLOW-UP PROBLEMS

17.1A <u>Plan:</u> First, balance the equations and then write the reaction quotient. Products appear in the numerator of the reaction quotient and reactants appear in the denominator; coefficients in the balanced reaction become exponents. <u>Solution:</u> a) Balanced equation:  $4NH_3(g) + 5O_2(g) \leftrightarrows 4NO(g) + 6H_2O(g)$ Reaction quotient:  $Q_c = \frac{[NO]^4 [H_2O]^6}{[NH_3]^4 [O_2]^5}$ 

b) Balanced equation:  $2NO_2(g) + 7H_2(g) \leftrightarrows 2NH_3(g) + 4H_2O(l)$ Reaction quotient:  $Q_c = \frac{[NH_3]^2}{[NO_2]^2[H_2]^7}$ 

c) Balanced equation:  $2\text{KCIO}_3(s) \leftrightarrows 2\text{KCl}(s) + 3\text{O}_2(g)$ Reaction quotient:  $Q_c = [\text{O}_2]^3$ 

17.1B <u>Plan:</u> First, balance the equations and then write the reaction quotient. Products appear in the numerator of the reaction quotient and reactants appear in the denominator; coefficients in the balanced reaction become exponents. <u>Solution:</u>

a) Balanced equation:  $CH_4(g) + CO_2(g) \leftrightarrows 2CO(g) + 2H_2(g)$ Reaction quotient:  $Q_c = \frac{[CO]^2[H_2]^2}{[CH_4][CO_2]}$ b) Balanced equation:  $2H_2S(g) + SO_2(g) \leftrightarrows 2S(s) + 2H_2O(g)$ Reaction quotient:  $Q_c = \frac{[H_2O]^2}{[H_2S]^2[SO_2]}$ c) Balanced equation:  $HCN(aq) + NaOH(aq)(s) \leftrightarrows NaCN(aq) + H_2O(l)$ Reaction quotient:  $Q_c = \frac{[NaCN]}{[HCN][NaOH]}$ 

- 17.2A <u>Plan:</u> Add the individual steps to find the overall equation, canceling substances that appear on both sides of the equation. Write the reaction quotient for each step and the overall equation. Multiply the reaction quotients for each step and cancel terms to obtain the overall reaction quotient. Solution:
  - $1 \qquad \qquad Br_2(g) \leftrightarrows 2Br(g)$
  - (2)  $\operatorname{Br}(g) + \operatorname{H}_2(g) \leftrightarrows \operatorname{HBr}(g) + \operatorname{H}(g)$
  - (3)  $\underline{\mathrm{H}}(g) + \mathrm{Br}(g) \leftrightarrows \mathrm{HBr}(g)$

 $\operatorname{Br}_2(g) + \frac{2\operatorname{Br}(g)}{2} + \operatorname{H}_2(g) + \frac{\operatorname{H}(g)}{4} \stackrel{\leftarrow}{\rightarrow} \frac{2\operatorname{Br}(g)}{2} + 2\operatorname{HBr}(g) + \frac{\operatorname{H}(g)}{4}$ 

Canceling the reactants leaves the overall equation as  $Br_2(g) + H_2(g) \leftrightarrows 2HBr(g)$ . Write the reaction quotients for each step:

$$Q_{c1} = \frac{\left[Br\right]^2}{\left[Br_2\right]} \qquad Q_{c2} = \frac{\left[HBr\right]\left[H\right]}{\left[Br\right]\left[H_2\right]} \qquad \qquad Q_{c3} = \frac{\left[HBr\right]}{\left[H\right]\left[Br\right]}$$

and for the overall equation:

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$$Q_{c} = \frac{\left[\mathrm{HBr}\right]^{2}}{\left[\mathrm{H}_{2}\right]\left[\mathrm{Br}_{2}\right]}$$

Multiplying the individual  $Q_c$ 's and canceling terms gives

$$Q_{c1} Q_{c2} Q_{c3} = \frac{\left[Br\right]^2}{\left[Br_2\right]} \times \frac{\left[HBr\right]\left[H\right]}{\left[Br\right]\left[H_2\right]} \times \frac{\left[HBr\right]}{\left[H\right]\left[Br\right]} = \frac{\left[HBr\right]^2}{\left[H_2\right]\left[Br_2\right]}$$

The product of the multiplication of the three individual reaction quotients equals the overall reaction quotient.

17.2B <u>Plan:</u> Add the individual steps to find the overall equation, canceling substances that appear on both sides of the equation. Write the reaction quotient for each step and the overall equation. Multiply the reaction quotients for each step and cancel terms to obtain the overall reaction quotient.

Solution:

(1) 
$$H_2(g) + ICl(g) \leftrightarrows HI(g) + HCl(g)$$

(2)  $\underline{\mathrm{HI}}(g) + \mathrm{ICl}(g) \leftrightarrows \underline{\mathrm{I}}_{2}(g) + \mathrm{HCl}(g)$ 

 $H_2(g) + 2ICl(g) + HI(g) \leftrightarrows HI(g) + 2HCl(g) + I_2(g)$ Canceling the reactants leaves the overall equation as  $H_2(g) + 2ICl(g) \leftrightarrows 2HCl(g) + I_2(g)$ Write the reaction quotients for each step:

$$Q_{c1} = \frac{[HI][HCI]}{[H2][ICI]} \quad Q_{c2} = \frac{[I_2][HCI]}{[HI][ICI]}$$

and for the overall equation:

$$Q_{\rm c} = \frac{[{\rm HCl}]^2 [{\rm I}_2]}{[{\rm H}_2] [{\rm ICl}]^2}$$

Multiplying the individual  $Q_c$ 's and canceling terms gives

$$Q_{c1} Q_{c2} = \frac{[\text{HI}][\text{HCI}]}{[\text{H}_2][\text{ICI}]} \times \frac{[\text{I}_2][\text{HCI}]}{[\text{HI}][\text{ICI}]} = \frac{[\text{HCI}]^2[\text{I}_2]}{[\text{H}_2][\text{ICI}]^2}$$

The product of the multiplication of the two individual reaction quotients equals the overall reaction quotient.

17.3A <u>Plan:</u> When a reaction is multiplied by a factor, the equilibrium constant is raised to a power equal to the factor. When a reaction is reversed, the reciprocal of the equilibrium constant is used as the new equilibrium constant. Solution:

a) All coefficients have been multiplied by the factor 1/2 so the equilibrium constant should be raised to the 1/2 power (which is the square root).

For reaction a)  $K_c = (7.6 \times 10^8)^{\frac{1}{2}} = 2.7568 \times 10^4 = 2.8 \times 10^4$ 

b) The reaction has been reversed so the new  $K_c$  is the reciprocal of the original equilibrium constant. The reaction has also been multiplied by a factor of 2/3, so the reciprocal of the original  $K_c$  must be raised to the 2/3 power.

For reaction b) 
$$K_{\rm c} = \left(\frac{1}{7.6 \,\mathrm{x} \,\mathrm{10^8}}\right)^{\frac{2}{3}} = 1.20076 \,\mathrm{x} \,\mathrm{10^{-6}} = 1.2 \,\mathrm{x} \,\mathrm{10^{-6}}$$

17.3B <u>Plan:</u> When a reaction is multiplied by a factor, the equilibrium constant is raised to a power equal to the factor. When a reaction is reversed, the reciprocal of the equilibrium constant is used as the new equilibrium constant. <u>Solution:</u>

a) All coefficients have been multiplied by the factor 2. Additionally, the reaction has been reversed. Therefore, the reciprocal of the equilibrium constant should be raised to the 2 power.

For reaction a)  $K_c = (1/1.3 \times 10^{-2})^2 = 5917.1598 = 5.9 \times 10^3$ 

b) All coefficients have been multiplied by the factor 1/4 so the equilibrium constant should be raised to the 1/4 power.

For reaction b) 
$$K_c = (1.3 \times 10^{-2})^{1/4} = 0.33766 = 0.34$$

17.4A <u>Plan:</u>  $K_p$  and  $K_c$  for a reaction are related through the ideal gas equation as shown in  $K_P = K_c (RT)^{\Delta n}$ . Find  $\Delta n_{gas}$ , the change in the number of moles of gas between reactants and products (calculated as products minus reactants). Then, use the given  $K_c$  to solve for  $K_p$ .

Solution:

The total number of product moles of gas is 1 and the total number of reactant moles of gas is 2.

$$\Delta n = 1 - 2 = -1$$
  
 $K_{\rm P} = K_{\rm c} (RT)^{\Delta n}$   
 $K_{\rm P} = 1.67[(0.0821 \text{ atm} \cdot \text{L/mol} \cdot \text{K})(500. \text{ K})]^{-1}$   
 $K_{\rm P} = 0.040682095 = 4.07 \times 10^{-2}$ 

17.4B <u>Plan:</u>  $K_p$  and  $K_c$  for a reaction are related through the ideal gas equation as shown in  $K_P = K_c (RT)^{\Delta n}$ . Find  $\Delta n_{gas}$ , the change in the number of moles of gas between reactants and products (calculated as products minus reactants). Then, use the given  $K_P$  to solve for  $K_c$ .

The total number of product moles of gas is 3 and the total number of reactant moles of gas is 5.

 $\Delta n = 3 - 5 = -2$   $K_{\rm P} = K_{\rm c} (RT)^{\Delta n}$   $K_{\rm P} = K_{\rm c} (RT)^{-2}$   $K_{\rm P} (RT)^{2} = K_{\rm c}$   $K_{\rm c} = (3.0 \times 10^{-5}) \left[ (0.0821 \text{ atm} \cdot \text{L/mol} \cdot \text{K}) (1173 \text{ K}) \right]^{2} = 0.27822976 = 0.28$ 

17.5A <u>Plan</u>: Write the reaction quotient for the reaction and calculate  $Q_c$  for each circle. Compare  $Q_c$  to  $K_c$  to determine the direction needed to reach equilibrium. If  $Q_c > K_c$ , reactants are forming. If  $Q_c < K_c$ , products are forming.

Solution:

The reaction quotient is  $\frac{[Y]}{[X]}$ .

Circle 1:  $Q_c = \frac{[Y]}{[X]} = \frac{[3]}{[9]} = 0.33$ Since  $Q_c < K_c$  (0.33 < 1.4), the reaction will shift to the **right** to reach equilibrium Circle 2:  $Q_c = \frac{[Y]}{[X]} = \frac{[7]}{[5]} = 1.4$ Since  $Q_c = K_c$  (1.4 = 1.4), there is **no change** in the reaction direction. The reaction is at equilibrium now. Circle 3:  $Q_c = \frac{[Y]}{[X]} = \frac{[8]}{[4]} = 2.0$ 

Since  $Q_c > K_c$  (2.0 > 1.4), the reaction will shift to the **left** to reach equilibrium

17.5B <u>Plan</u>: Write the reaction quotient for the reaction and calculate  $Q_c$  for each circle. Compare  $Q_c$  to  $K_c$  to determine the direction needed to reach equilibrium. If  $Q_c > K_c$ , reactants are forming. If  $Q_c < K_c$ , products are forming.

Solution:

The reaction quotient is  $\frac{[D]}{[C]^2}$ . Circle 1:  $Q_c = \frac{[D]}{[C]^2} = \frac{[5]}{[3]^2} = 0.56$ According to the problem, circle 1 is at equilibrium. Therefore,  $K_c = 0.56$ . Circle 2:  $Q_c = \frac{[D]}{[C]^2} = \frac{[6]}{[3]^2} = 0.67$ Since  $Q_c > K_c$  (0.67 > 0.56), the reaction will shift to the **left** to reach equilibrium. Circle 3:  $Q_c = \frac{[D]}{[C]^2} = \frac{[7]}{[4]^2} = 0.44$ Since  $Q_c < K_c$  (0.44 < 0.56), the reaction will shift to the **right** to reach equilibrium

17.6A <u>Plan:</u> To decide whether  $CH_3Cl$  or  $CH_4$  are forming while the reaction system moves toward equilibrium, calculate  $Q_p$  and compare it to  $K_p$ . If  $Q_p > K_p$ , reactants are forming. If  $Q_p < K_p$ , products are forming. <u>Solution:</u>

$$Q_{\rm P} = \frac{P_{\rm CH_3Cl}P_{\rm HCl}}{P_{\rm CH_4}P_{\rm Cl_2}} = \frac{(0.24\,\rm{atm})(0.47\,\rm{atm})}{(0.13\,\rm{atm})(0.035\,\rm{atm})} = 24.7912 = 25$$

 $K_p$  for this reaction is given as 1.6x10<sup>4</sup>.  $Q_p$  is smaller than  $K_p$  ( $Q_p < K_p$ ) so more products will form. **CH<sub>3</sub>Cl** is one of the products forming.

17.6B <u>Plan</u>: To determine whether the reaction is at equilibrium or, if it is not at equilibrium, which direction to will proceed, calculate  $Q_c$  and compare it to  $K_c$ . If  $Q_c > K_c$ , the reaction will proceed to the left. If  $Q_c < K_c$ , the reaction will proceed to the right.

Solution:

$$Q_{c} = \frac{\left[SO_{3}\right]^{2}}{\left[SO_{2}\right]^{2}\left[O_{2}\right]} = \frac{\left[\frac{1.2 \text{ mol}}{2.0 \text{ L}}\right]^{2}}{\left[\frac{3.4 \text{ mol}}{2.0 \text{ L}}\right]^{2}\left[\frac{1.5 \text{ mol}}{2.0 \text{ L}}\right]} = 0.166089965 = 0.17$$

The system is **not at equilibrium**.  $K_c$  for this reaction is given as 4.2 x 10<sup>-2</sup>.  $Q_c$  is larger than  $K_c$  ( $Q_c > K_c$ ) so the reaction will proceed to the **left**.

- 17.7A <u>Plan:</u> The information given includes the balanced equation, initial pressures of both reactants, and the equilibrium pressure for one reactant. First, set up a reaction table showing initial partial pressures for reactants and 0 for product. The change to get to equilibrium is to react some of reactants to form some product. Use the equilibrium quantity for  $O_2$  and the expression for  $O_2$  at equilibrium to solve for the change. From the change find the equilibrium partial pressure for NO and NO<sub>2</sub>. Calculate  $K_p$  using the equilibrium values. Solution:
  - Pressures (atm)2NO(g)+  $O_2(g)$  $\leftrightarrows$  $2NO_2(g)$ Initial1.0001.0000Change-2x-x+2xEquilibrium1.000 2x1.000 x2xAt equilibrium $P_{O_2} = 0.506$  atm = 1.000 x; so x = 1.000 0.506 = 0.494 atm $P_{NO} = 1.000 2x = 1.000 2(0.494) = 0.012$  atm $P_{NO_2} = 2x = 2(0.494) = 0.988$  atm

Use the equilibrium pressures to calculate  $K_p$ .

$$K_{\rm P} = \frac{P_{\rm NO_2}^2}{P_{\rm NO}^2 P_{\rm O_2}} = \frac{\left(0.988\right)^2}{\left(0.012\right)^2 \left(0.506\right)} = 1.339679 \, \mathrm{x10^4} = 1.3 \mathrm{x10^4}$$

17.7B <u>Plan</u>: The information given includes the balanced equation, initial concentrations of both reactants, and the equilibrium concentration for one product. First, set up a reaction table showing initial concentrations for reactants and 0 for products. The change to get to equilibrium is to react some of reactants to form some of the products. Use the equilibrium quantity for  $N_2O_4$  and the expression for  $N_2O_4$  at equilibrium to solve for the change. From the change find the equilibrium concentrations for NH<sub>3</sub>, O<sub>2</sub>, and H<sub>2</sub>O. Calculate  $K_c$  using the equilibrium values. <u>Solution</u>:

Pressures (atm) 
$$4NH_3(g) + 7O_2(g) \leftrightarrows 2N_2O_4(g) + 6H_2O(g)$$
  
Initial 2.40 2.40 0 0  
Change  $-4x$   $-7x$   $+2x$   $+6x$   
Equilibrium 2.40  $-4x$  2.40  $-7x$  2x 6x  
At equilibrium  $[N_2O_4] = 0.134 M = 2x$ ; so  $x = 0.0670 M$   
 $[NH_3] = 2.40 M - 4(0.0670 M) = 2.13 M$   
 $[O_2] = 2.40 M - 7(0.0670 M) = 1.93 M$   
 $[H_2O] = 6(0.0670 M) = 0.402 M$   
Use the equilibrium pressures to calculate  $K_c$ .  
 $K_c = \frac{[N_2O_4]^2[H_2O]^6}{[NH_3]^4[O_2]^7} = \frac{(0.134)^2(0.402)^6}{(2.13)^4(1.93)^7} = 3.6910x10^{-8} = 3.69x10^{-8}$ 

17.8A <u>Plan:</u> Convert  $K_c$  to  $K_p$  for the reaction. Write the equilibrium expression for  $K_p$  and insert the atmospheric pressures for  $P_{N_2}$  and  $P_{O_2}$  as their equilibrium values. Solve for  $P_{NO}$ .

The conversion of  $K_c$  to  $K_p$ :  $K_p = K_c (RT)^{\Delta n}$ . For this reaction  $\Delta n = 0$ , so  $K_p = K_c$ .  $K_P = \frac{P_{N_2} P_{O_2}}{R_c^2} = K_c = 2.3 \times 10^{30} = \frac{(0.781)(0.209)}{2}$ 

$$P_{\rm NO}^2$$
 x<sup>2</sup>  
x = 2.6640x10<sup>-16</sup> = 2.7x10<sup>-16</sup> atm

The equilibrium partial pressure of NO in the atmosphere is  $2.7 \times 10^{-16}$  atm.

17.8B <u>Plan:</u> Write the equilibrium expression for  $K_p$  and insert the partial pressures for PH<sub>3</sub> and P<sub>2</sub> as their equilibrium values. Solve for the partial pressure of H<sub>2</sub>. <u>Solution:</u>

$$K_{\rm P} = \frac{(P_{\rm P_2})(P_{\rm H_2})^3}{(P_{\rm PH_3})^2} = \sqrt[3]{\frac{K_{\rm P}(P_{\rm PH_3})^2}{(P_{\rm P_2})}} = P_{\rm H_2} = \sqrt[3]{\frac{(19.6)(0.112)^2}{(0.215)}} = 1.0457 = 1.05 \text{ atm}$$

17.9A <u>Plan:</u> Find the initial molarity of HI by dividing moles of HI by the volume. Set up a reaction table and use the variables to find equilibrium concentrations in the equilibrium expression. Solution:

$$\begin{split} M_{\rm HI} &= \frac{\text{moles HI}}{\text{volume}} = \frac{2.50 \text{ mol}}{10.32 \text{ L}} = 0.242248 M \\ \text{Concentration } (M) & 2\text{HI}(g) &\leftrightarrows & \text{H}_2(g) + \text{I}_2(g) \\ \text{Initial} & 0.242248 & 0 & 0 \\ \hline \text{Change} & -2x & +x & +x \\ \hline \text{Equilibrium} & 0.242248 - 2x & x & x \\ \text{Set up equilibrium expression:} \\ K_c &= 1.26x10^{-3} = \frac{\left[\text{H}_2\right]\left[\text{I}_2\right]}{\left[\text{HI}\right]^2} = \frac{\left[x\right]\left[x\right]}{\left[0.242248 - 2x\right]^2} \\ 3.54965x10^{-2} &= \frac{\left[x\right]}{\left[0.242248 - 2x\right]} \\ x &= 8.59895x10^{-3} - 7.0993x10^{-2} x \\ x &= 8.02895x10^{-3} = 8.03x10^{-3} \\ \hline \text{H}_2 &= \left[\text{I}_2\right] = 8.02x10^{-3} M \end{split}$$

17.9B <u>Plan:</u> Find the initial molarities of Cl<sub>2</sub>O and H<sub>2</sub>O by dividing moles by the volume of the flask. Set up a reaction table and use the variables to find equilibrium concentrations in the equilibrium expression. Solution:

Molarity of Cl<sub>2</sub>O = 
$$\frac{\text{moles Cl}_2O}{\text{volume}}$$
 =  $\frac{6.15 \text{ mol}}{5.00 \text{ L}}$  = 1.23 M  
Molarity of H<sub>2</sub>O =  $\frac{\text{moles H}_2O}{\text{volume}}$  =  $\frac{6.15 \text{ mol}}{5.00 \text{ L}}$  = 1.23 M  
Concentration (M) Cl<sub>2</sub>O(g) + H<sub>2</sub>O(g)  $\Rightarrow$  2HOCl (g)  
Initial 1.23 1.23 0  
Change -x -x +2x  
Equilibrium 1.23 - x 1.23 - x 2x  
Set up equilibrium expression:  
 $K_c = 0.18 = \frac{[\text{HOCl}]^2}{[\text{Cl}_2O][\text{H}_2O]} = \frac{[2x]^2}{[1.23 - x][1.23 - x]}$ 

Take the square root of each side.  $0.424264068 = \frac{[2x]}{[1.23 - x]}$ 0.521844804 - 0.424264068x = 2x0.521844804 = 2.424264068xx = 0.215259000 = 0.21 M $[Cl_2O] = [H_2O] = 1.23 M - 0.21 M = 1.02 M$ [HOC1] = 2(0.21 M) = 0.42 M

17.10A Plan: Find the molarity of  $I_2$  by dividing moles of  $I_2$  by the volume. First set up the reaction table, then set up the equilibrium expression. To solve for the variable, x, first assume that x is negligible with respect to initial concentration of  $I_2$ . Check the assumption by calculating the % error. If the error is greater than 5%, calculate x using the quadratic equation. The next step is to use x to determine the equilibrium concentrations of  $I_2$  and I. Solution:

$$[I_2]_{\text{init}} = \frac{0.50 \text{ mol}}{2.5 \text{ L}} = 0.20 M$$

a) Equilibrium at 600 K

Concentration ( <i>M</i> )	$I_2(g) \leftrightarrows$	2I(g)
Initial	0.20	0
Change	—X	+2x
Equilibrium	0.20 - x	2x
	<b>5 3</b> <sup>2</sup>	

Equilibrium expression:  $K_c = \frac{\lfloor I \rfloor^-}{\lfloor I_2 \rfloor} = 2.94 \times 10^{-10}$ 

 $\frac{[2x]^2}{[0.20 - x]} = 2.94 \times 10^{-10}$  Assume x is negligible so  $0.20 - x \approx 0.20$  $\frac{\left[2x\right]^2}{\left[0.20\right]} = 2.94 \times 10^{-10}$  $4x^{2} = (2.94x10^{-10}) (0.20); x = 3.834x10^{-6} = 3.8x10^{-6}$ 

Check the assumption by calculating the % error:

$$\frac{3.8 \times 10^{-6}}{(100)}$$

 $\frac{0.010}{0.20}$  (100) = 0.0019% which is smaller than 5%, so the assumption is valid.

At equilibrium  $[I]_{eq} = 2x = 2(3.8 \times 10^{-6}) = 7.668 \times 10^{-6} = 7.7 \times 10^{-6} M$  and  $[I_2]_{eq} = 0.20 - x = 0.20 - 3.834 \times 10^{-6} = 0.199996 = 0.20 M$ 

b) Equilibrium at 2000 K

Equilibrium expression:  $K_{\rm c} = \frac{\left[I\right]^2}{\left[I_2\right]} = 0.209$  $\frac{[2x]^2}{[0.20 - x]} = 0.209$  Assume x is negligible so 0.20 - x is approximately 0.20  $\frac{\left[2x\right]^2}{\left[0.20\right]} = 0.209$  $4x^2 = (0.209)(0.20)$ x = 0.102225 = 0.102Check the assumption by calculating the % error:

 $\frac{0.102}{0.20}(100) = 51\%$  which is larger than 5% so the assumption is not valid. Solve using quadratic equation.

$$\frac{\left[2x\right]^{2}}{\left[0.20-x\right]} = 0.209$$

$$4x^{2} + 0.209x - 0.0418 = 0$$

$$x = \frac{-0.209 \pm \sqrt{\left(0.209\right)^{2} - 4\left(4\right)\left(-0.0418\right)}}{2(4)} = 0.0793857 \text{ or } -0.1316$$
Choose the positive value,  $x = 0.079$ 

At equilibrium  $[I]_{eq} = 2x = 2(0.079) = 0.15877 = 0.16 M$  and  $[I_2]_{eq} = 0.20 - x = 0.20 - 0.079 = 0.12061 = 0.12 M$ 

17.10B <u>Plan:</u> First set up the reaction table, then set up the equilibrium expression. To solve for the variable, x, first assume that x is negligible with respect to initial partial pressure of PCl<sub>5</sub>. Check the assumption by calculating the % error. If the error is greater than 5%, calculate x using the quadratic equation. The next step is to use x to determine the equilibrium partial pressure of PCl<sub>5</sub>. <u>Solution:</u>

a) Equilibrium at a PCl<sub>5</sub> partial pressure of 0.18 atm:

	Partial Pressure (atm)	$PCl_5(g) \leftrightarrows$	$PCl_3(g) +$	$\operatorname{Cl}_2(g)$
	Initial	0.18	0	0
	Change	X	+x +x	
	Equilibrium	0.18 - x	X	Х
	Equilibrium expression: $K_{\rm P} = \frac{(P_{\rm P})}{(P_{\rm P})^2}$	$\frac{(P_{Cl_3})(P_{Cl_2})}{(P_{PCl_5})} = 3.4x$	10 <sup>-4</sup>	
	$\frac{(x)(x)}{(0.18 - x)} = 3.4x10^{-4} \text{ Ass}$ $\frac{(x)(x)}{(0.18)} = 3.4x10^{-4}$	ume x is negligibl	e so $0.18 - x \approx 0.1$	8
	$x^{2} = (3.4x10^{-4}) (0.18); x =$	= 0.0078230428 =	$7.8 \times 10^{-3}$	
	Check the assumption by calculating	ng the % error:		
	$\frac{7.8 \times 10^{-3}}{0.18} (100) = 4.3\% \text{ which is smaller}$ At equilibrium [PCl <sub>5</sub> ] <sub>eq</sub> = 0.18 <i>M</i> -	aller than 5%, so the formula of $-7.8 \ge 10^{-3} M = 0.000$	ne assumption is va 17 <i>M</i>	alid.
b) Equil	ibrium at a PCl <sub>5</sub> partial pressure of	0.18 atm:		
	Partial Pressure (atm)	$PCI_5(g) \rightarrow 0.025$	$PCI_3(g) + 0$	$Cl_2(g)$
	Change	0.025	0	0
	Equilibrium	$-\lambda$	τ <u>λ</u> v	<u>+</u> <u></u>
	Equilionum	0.023 - x	Χ	X
	Equilibrium expression: $K_{\rm P} = \frac{(P)}{(P)}$	$\frac{(P_{Cl_3})(P_{Cl_2})}{(P_{P_{Cl_5}})} = 3.4x^{-1}$	10 <sup>-4</sup>	
	$\frac{(x)(x)}{(0.025 - x)} = 3.4x10^{-4} \text{ As}$	sume x is negligib	the so $0.025 - x \approx 0$	0.025
	$\frac{(x)(x)}{(0.025)} = 3.4 \times 10^{-4}$			
	(0.025) $y^2 = (2.4y10^{-4})(0.025); y$	- 0.002015476- "	$0_{\rm W} 10^{-3}$	
	$X = (3.4X10^{\circ})(0.023), X$	= 0.002913470 - 2	2.9X10	
		ing the % error.		
	$\frac{2.9 \times 10^{-5}}{0.025}$ (100) = 12% which is larg equation.	er than 5%, so the	assumption is NC	)T valid. Solve using quadratic
	$(x)(x) = 2.4 \times 10^{-4}$			

 $\frac{1}{(0.025-x)} = 3.4x10^{-1}$ 

$$x^{2} + 3.4x10^{-4}x - 8.5x10^{-6} = 0$$
  
$$x = \frac{+8.5x10^{-6} \pm \sqrt{(3.4x10^{-4})^{2} - 4(1)(-8.5x10^{-6})}}{2(1)} = 0.002750428051 \text{ or } -0.003090428051$$

Choose the positive value, x = 0.0028 M; At equilibrium  $[PCl_5]_{eq} = 0.025 M - 0.0028 M = 0.022 M$ 17.11A Plan: Calculate the initial concentrations (molarity) of each substance. For part (a), calculate  $Q_c$  and compare to given  $K_c$ . If  $Q_c > K_c$  then the reaction proceeds to the left to make reactants from products. If  $Q_c < K_c$  then the reaction proceeds to right to make products from reactants. For part (b), use the result of part (a) and the given equilibrium concentration of PCl<sub>5</sub> to find the equilibrium concentrations of PCl<sub>3</sub> and Cl<sub>2</sub>.

Solution:

 $[PCl_5] = \frac{0.1050 \text{ mol}}{0.5000 \text{ L}} = 0.2100 M$ Initial concentrations:  $[PCl_3] = [Cl_2] = \frac{0.0450 \text{ mol}}{0.5000 \text{ L}} = 0.0900 \text{ M}$ a)  $Q_{\rm c} = \frac{\left[\text{PCl}_3\right]\left[\text{Cl}_2\right]}{\left[\text{PCl}_5\right]} = \frac{\left[0.0900\right]\left[0.0900\right]}{\left[0.2100\right]} = 0.038571 = 0.0386$ 

 $Q_c$ , 0.0386, is less than  $K_c$ , 0.042, so the reaction will proceed to the **right** to make more products. b) To reach equilibrium, concentrations will increase for the products, PCl<sub>3</sub> and Cl<sub>2</sub>, and decrease for the reactant, PCl<sub>5</sub>. Con

centration (M)	$PCl_5(g)$	╘	$PCl_3(g) +$	$\operatorname{Cl}_2(g)$
Initial	0.2100		0.0900	0.0900
Change	—X		+x	+x
Equilibrium	0.2100 - x		0.0900 + x	0.0900 + x

$$[PCl_5] = 0.2065 = 0.2100 - x; x = 0.0035 M$$
$$[PCl_3] = [Cl_2] = 0.0900 + x = 0.0900 + 0.0035 = 0.0935 M$$

17.11B Plan: For part (a), calculate  $Q_P$  and compare to given  $K_P$ . If  $Q_P > K_P$  then the reaction proceeds to the left to make reactants from products. If  $Q_{\rm P} < K_{\rm P}$  then the reaction proceeds to right to make products from reactants. For part (b), set up a reaction table and use the variables to find equilibrium concentrations in the equilibrium expression. Solution:

$$Q_{\rm P} = \frac{(P_{\rm NO})^2}{(P_{\rm N2})(P_{\rm O2})} = \frac{(0.750)^2}{(0.500)(0.500)} = 2.25$$

 $Q_{\rm P}$ , 2.25, is greater than  $K_{\rm P}$ , 8.44 x 10<sup>-3</sup>, so the reaction will proceed to the **left** to make more reactants. To reach equilibrium, concentrations will increase for the reactants,  $N_2$  and  $O_2$ , and decrease for the product, NO.

· · · · · · · · · · · · · · · · · · ·			,	,
Pressure (atm)	$N_2(g) +$	$O_2(g)$	与	2NO (g)
Initial	0.500	0.500		0.750
Change	$+\mathbf{x}$	+x		-2x
Equilibrium	0.500 + x	0.500 + x		0.750 - 2 x
$K_{\rm P} = \frac{(P_{\rm NO})^2}{(P_{\rm N2})(P_{\rm O2})} = \frac{(0.750)}{(0.500 + x)^2}$	$\frac{(0-2x)^2}{(0.500+x)} = 8.44x10$	)-3		
Take the square root of each	ı side.			
$\frac{(0.750-2x)}{(0.750-x)} = 0.0919$				
$(U \supset UU + X)$				

(0.500 + x)0.750 - 2x = 0.0460 + 0.0919x0.704 = 2.0919xx = 0.337 M $[N_2] = [O_2] = 0.500 M + 0.337 M = 0.837 M$ [NO] = 0.750 M - 2(0.337 M) = 0.076 M

17.12A <u>Plan</u>: Examine each change for its impact on  $Q_c$ . Then decide how the system would respond to re-establish equilibrium.

Solution:

$$Q_{\rm c} = \frac{\left[\mathrm{SiF}_4\right] \left[\mathrm{H}_2\mathrm{O}\right]^2}{\left[\mathrm{HF}\right]^4}$$

a) Decreasing [H<sub>2</sub>O] leads to  $Q_c < K_c$ , so the reaction would shift to make more products from reactants. Therefore, the SiF<sub>4</sub> concentration, as a product, would **increase**.

b) Adding liquid water to this system at a temperature above the boiling point of water would result in an increase in the concentration of water vapor. The increase in [H<sub>2</sub>O] increases  $Q_c$  to make it greater than  $K_c$  To re-establish equilibrium products will be converted to reactants and the [SiF<sub>4</sub>] will decrease.

c) Removing the reactant HF increases  $Q_c$ , which causes the products to react to form more reactants. Thus, [SiF<sub>4</sub>] decreases.

d) Removal of a solid product has no impact on the equilibrium;  $[SiF_4]$  does not change.

Check: Look at each change and decide which direction the equilibrium would shift using Le Châtelier's principle to check the changes predicted above.

- a) Remove product, equilibrium shifts to right.
- b) Add product, equilibrium shifts to left.
- c) Remove reactant, equilibrium shifts to left.
- d) Remove solid reactant, equilibrium does not shift.
- 17.12B Plan: Examine each change for its impact on  $Q_c$ . Then decide how the system would respond to re-establish equilibrium.

Solution:

 $\overline{Q_{\rm c}} = \frac{[\rm CO][\rm H_2]}{[\rm H_2O]}$ 

a) Adding carbon, a solid reactant, has no impact on the equilibrium. [CO] does not change.

b) Removing water vapor, a reactant, increases  $Q_c$ , which causes the products to react to form more reactants. Thus, [CO] decreases.

c) Removing the product  $H_2$  decreases  $Q_c$ , which causes the reactants to react to form more products. Thus, [CO] increases.

d) Adding water vapor, a reactant, decreases  $Q_c$ , which causes the reactants to react to form more products. Thus, [CO] increases.

Check: Look at each change and decide which direction the equilibrium would shift using Le Châtelier's principle to check the changes predicted above.

- a) Add solid reactant, equilibrium does not shift.
- b) Remove reactant, equilibrium shifts to the left.
- c) Remove product, equilibrium shifts to the right.
- d) Add reactant, equilibrium shifts to the right.
- 17.13A Plan: Changes in pressure (and volume) affect the concentration of gaseous reactants and products. A decrease in pressure, i.e., increase in volume, favors the production of more gas molecules whereas an increase in pressure favors the production of fewer gas molecules. Examine each reaction to decide whether more or fewer gas molecules will result from producing more products. If more gas molecules result, then the pressure should be increased (volume decreased) to reduce product formation. If fewer gas molecules result, then pressure should be decreased to produce more reactants.

Solution:

a) In  $2SO_2(g) + O_2(g) \rightleftharpoons 2SO_3(g)$  three molecules of gas form two molecules of gas, so there are fewer gas molecules in the product. Decreasing pressure (increasing volume) will decrease the product yield. b) In  $4NH_3(g) + 5O_2(g) \Rightarrow 4NO(g) + 6H_2O(g)$  9 molecules of reactant gas convert to 10 molecules of product gas. Increasing pressure (decreasing volume) will favor the reaction direction that produces fewer moles of gas: towards the reactants and away from products.

c) In CaC<sub>2</sub>O<sub>4</sub>(s)  $\Rightarrow$  CaCO<sub>3</sub>(s) + CO(g) there are no reactant gas molecules and one product gas molecule. The yield of the products will decrease when volume decreases, which corresponds to a pressure increase.

17.13B <u>Plan:</u> Changes in pressure (and volume) affect the concentration of gaseous reactants and products. A decrease in pressure, i.e., increase in volume, favors the production of more gas molecules whereas an increase in pressure favors the production of fewer gas molecules. Examine each reaction to determine if a decrease in pressure will shift the reaction toward the products (resulting in an increase in the yield of products) or toward the reactants (resulting in a decrease in the yield of products). Solution:

a) In  $CH_4(g) + CO_2(g) \leftrightarrows 2CO(g) + 2H_2(g)$  two molecules of gas form four molecules of gas, so there are more gas molecules in the product. Decreasing pressure (increasing volume) will shift the reaction to the right, **increasing** the product yield.

b) In NO(g) + CO<sub>2</sub>(g)  $\leftrightarrows$  NO<sub>2</sub>(g) + CO(g) 2 molecules of reactant gas convert to 2 molecules of product gas. Decreasing pressure (increasing volume) will have **no effect** on this reaction or on the amount of product produced because the number of moles of gas does not change.

c) In  $2H_2S(g) + SO_2(g) \Rightarrow 3S(s + 2H_2O(g))$  three molecules of reactant gas convert to 2 molecules of product gas. Decreasing pressure (increasing volume) will shift the reaction toward the reactants, **decreasing** the product yield.

17.14A <u>Plan</u>: A decrease in temperature favors the exothermic direction of an equilibrium reaction. First, identify whether the forward or reverse reaction is exothermic from the given enthalpy change.  $\Delta H < 0$  means the forward reaction is exothermic, and  $\Delta H > 0$  means the reverse reaction is exothermic. If the forward reaction is exothermic then a decrease in temperature will shift the equilibrium to make more products from reactants and increase  $K_p$ . If the reverse reaction is exothermic then a decrease in temperature will shift the a decrease in temperature will shift the advectage in temperature will shift the equilibrium to make more reactants from products and decrease  $K_p$ .

Solution:

a)  $\Delta H < 0$  so the forward reaction is exothermic. A decrease in temperature increases the partial pressure of products and decreases the partial pressures of reactants, so  $P_{\rm H_2}$  decreases. With increases in product pressures

and decreases in reactant pressures,  $K_p$  increases.

b)  $\Delta H > 0$  so the reverse reaction is exothermic. A decrease in temperature decreases the partial pressure of products and increases the partial pressures of reactants, so  $P_{N_2}$  increases.  $K_p$  decreases with decrease in product

pressures and increase in reactant pressures.

c)  $\Delta H < 0$  so the forward reaction is exothermic. Decreasing temperature increases  $P_{PCl_5}$  and increases  $K_p$ .

17.14B <u>Plan</u>: A decrease in temperature favors the exothermic direction of an equilibrium reaction. First, identify whether the forward or reverse reaction is exothermic from the given enthalpy change.  $\Delta H < 0$  means the forward reaction is exothermic, and  $\Delta H > 0$  means the reverse reaction is exothermic. If the forward reaction is exothermic then a decrease in temperature will shift the equilibrium to make more products from reactants and increase  $K_p$ . If the reverse reaction is exothermic then an increase in temperature will shift the equilibrium to make more products from reactants and increase  $K_p$ .

Solution:

a)  $\Delta H > 0$  so the reverse reaction is exothermic. An **increase in temperature** will increase the partial pressure of products and decrease the partial pressures of reactants.  $K_p$  increases with an increase in product pressures and a decrease in reactant pressures.

b)  $\Delta H < 0$  so the forward reaction is exothermic. A **decrease in temperature** increases the partial pressure of products and decreases the partial pressures of reactants. With increases in product pressures and decreases in reactant pressures,  $K_p$  increases.

c)  $\Delta H > 0$  so the reverse reaction is exothermic. An **increase in temperature** increases the partial pressure of products and decreases the partial pressures of reactants.  $K_p$  increases with an increase in product pressures and a decrease in reactant pressures.

17.15A <u>Plan</u>: Given the balanced equilibrium equation, it is possible to set up the appropriate equilibrium expression  $(Q_c)$ . For the equation given  $\Delta n = 0$  meaning that  $K_p = K_c$ . The value of *K* may be found for scene 1, and values for *Q* may be determined for the other two scenes. The reaction will shift towards the reactant side if Q > K, and the reaction will shift towards the product side if Q < K. The reaction is exothermic ( $\Delta H < 0$ ), thus, heat may be considered a product. Increasing the temperature adds a product and decreasing the temperature removes a product.

#### Solution:

a)  $K_p$  requires the equilibrium value of *P* for each gas. The pressure may be found from P = nRT/V.

$$K_{\rm p} = \frac{P_{\rm CD}^2}{P_{\rm C_2} P_{\rm D_2}} = \frac{\left(\frac{n_{\rm CD} RT}{V}\right)^2}{\left(\frac{n_{\rm C_2} RT}{V}\right) \left(\frac{n_{\rm D_2} RT}{V}\right)}$$

This equation may be simplified because for the sample R, T, and V are constant. Using scene 1:

$$K_{\rm p} = \frac{n_{\rm CD}^2}{n_{\rm C_2} n_{\rm D_2}} = \frac{(4)^2}{(2)(2)} = 4$$

b) Scene 2:  $Q_{\rm p} = \frac{n_{\rm CD}^2}{n_{\rm C_2} n_{\rm D_2}} = \frac{(6)^2}{(1)(1)} = 36$ 

Q > K so the reaction will shift to the **left** (towards the reactants).

Scene 3: 
$$Q_{\rm p} = \frac{n_{\rm CD}^2}{n_{\rm C_2} n_{\rm D_2}} = \frac{(2)^2}{(3)(3)} = 0.44$$

Q < K so the reaction will shift to the **right** (towards the products).

c) Increasing the temperature is equivalent to adding a product (heat) to the equilibrium. The reaction will shift to consume the added heat. The reaction will shift to the left (towards the reactants). However, since there are 2 moles of gas on each side of the equation, the shift has **no effect** on total moles of gas.

17.15B <u>Plan</u>: Write the equilibrium expression for the reaction. Count the number of each type of particle in the first scene and use this information to calculate the value of *K* at  $T_1$ . Follow a similar procedure to calculate the value of *K* at  $T_2$ . Determine if *K* at  $T_1$  is larger or smaller than *K* at  $T_2$ . Use this information to determine the sign of  $\Delta H$  for the reaction.

Solution:  
a) 
$$K = \frac{[AB]}{[A][B]}$$
  
Calculating K at  $T_1$ :  
 $K = \frac{[3]}{[2][2]} = 0.75$   
b) Coince from the set

b) Going from the scene at  $T_1$  to the scene at  $T_2$ , the number of product molecules decreases. This decreases the value of *K*. The problem states that  $T_2 < T_1$ , so as the temperature decreases, *K* also decreases. The fact that both the temperature and the value of *K* decreased suggests that this is an endothermic reaction, with  $\Delta H > 0$ . c) Calculating *K* at  $T_2$ :

$$K = \frac{[2]}{[3][3]} = 0.22$$

#### CHEMICAL CONNECTIONS BOXED READING PROBLEM

B17.1 <u>Plan:</u> To control the pathways, the first enzyme specific for a branch is inhibited by the end product of that branch.

Solution:

a) The enzyme that is inhibited by F is the first enzyme in that branch, which is enzyme 3.

b) Enzyme **6** is inhibited by I.

c) If F inhibited enzyme 1, then neither branch of the reaction would take place once enough F was produced.

d) If F inhibited enzyme 6, then the second branch would not take place when enough F was made.

## **END-OF-CHAPTER PROBLEMS**

 $H_2$ 

17.1 If the rate of the forward reaction exceeds the rate of reverse reaction, products are formed faster than they are consumed. The change in reaction conditions results in more products and less reactants. A change in reaction conditions can result from a change in concentration or a change in temperature. If concentration changes, product concentration increases while reactant concentration decreases, but the  $K_c$  remains unchanged because the *ratio* of products and reactants remains the same. If the increase in the forward rate is due to a change in temperature, the rate of the reverse reaction also increases. The equilibrium ratio of product concentration to reactant concentration is no longer the same. Since the rate of the forward reaction increases more than the rate of the reverse reaction,  $K_c$  increases (numerator, [products], is larger and denominator, [reactants], is smaller).

$$K_{\rm c} = \frac{\left[ \text{products} \right]}{\left[ \text{reactants} \right]}$$

- 17.2 The faster the rate and greater the yield, the more useful the reaction will be to the manufacturing process.
- 17.3 A system at equilibrium continues to be very dynamic at the molecular level. Reactant molecules continue to form products, but at the same rate that the products decompose to re-form the reactants.
- 17.4 If *K* is very large, the reaction goes nearly to completion. A large value of *K* means that the numerator is much larger than the denominator in the *K* expression. A large numerator, relative to the denominator, indicates that most of the reactants have reacted to become products.  $K = \frac{[\text{products}]}{[\text{reactants}]}$
- 17.5 One cannot say with certainty whether the value of *K* for the phosphorus plus oxygen reaction is large or small (although it likely is large). However, it is certain that the reaction proceeds very fast.
- 17.6 No, the value of Q is determined by the mass action expression with arbitrary concentrations for products and reactants. Thus, its value is not constant.
- 17.7 The equilibrium constant expression is  $K = [O_2]$  (we do not include solid substances in the equilibrium expression). If the temperature remains constant, *K* remains constant. If the initial amount of Li<sub>2</sub>O<sub>2</sub> present was sufficient to reach equilibrium, the amount of O<sub>2</sub> obtained will be constant, regardless of how much Li<sub>2</sub>O<sub>2</sub>(*s*) is present.
- 17.8 a) On the graph, the concentration of HI increases at twice the rate that  $H_2$  decreases because the stoichiometric ratio in the balanced equation is  $1H_2$ : 2HI. Q for a reaction is the ratio of concentrations of products to concentrations of reactants. As the reaction progresses the concentration of reactants  $H_2$  and  $I_2$  decrease and the concentration of product HI increases, which means that Q increases as a function of time.

$$(g) + I_2(g) \leftrightarrows 2HI(g) \qquad Q = \frac{\left[HI\right]^2}{\left[H_2\right]\left[I_2\right]}$$
Output



The value of Q increases as a function of time until it reaches the value of K.

b) No, Q would still increase with time because the [I<sub>2</sub>] would decrease in exactly the same way as [H<sub>2</sub>] decreases.

17.9 A homogeneous equilibrium reaction exists when **all** the components of the reaction are in the same phase (i.e., gas, liquid, solid, aqueous).

 $2NO(g) + O_2(g) \leftrightarrows 2NO_2(g)$ 

A heterogeneous equilibrium reaction exists when the components of the reaction are in different phases.  $Ca(HCO_3)_2(aq) \leftrightarrows CaCO_3(s) + H_2O(l) + CO_2(g)$ 

17.10 
$$1/2N_2(g) + 1/2O_2(g) \rightleftharpoons NO(g)$$
  
 $Q_{c(form)} = \frac{[NO]}{[N_2]^{1/2}[O_2]^{1/2}}$   
 $NO(g) \leftrightarrows 1/2N_2(g) + 1/2O_2(g)$   
 $Q_{c(decomp)} = \frac{[N_2]^{1/2}[O_2]^{1/2}}{[NO]}$ 

 $Q_{c(decomp)} = 1/Q_{c(form)}$ , so the constants do differ (they are the reciprocal of each other).

17.11 <u>Plan:</u> Write the reaction and then the expression for Q. Remember that  $Q = \frac{\left[C\right]^{c} \left[D\right]^{d}}{\left[A\right]^{a} \left[B\right]^{b}}$  where A and B are

reactants, C and D are products, and *a*, *b*, *c*, and *d* are the stoichiometric coefficients in the balanced equation. Solution:

The balanced equation for the first reaction is

 $3/2H_2(g) + 1/2N_2(g) \leftrightarrows NH_3(g)$  (1)

The coefficient in front of  $NH_3$  is fixed at 1 mole according to the description. The reaction quotient for this  $\lceil NH_3 \rceil$ 

reaction is 
$$Q_1 = \frac{\left[ \mathbf{N}\mathbf{H}_3 \right]}{\left[ \mathbf{H}_2 \right]^{3/2} \left[ \mathbf{N}_2 \right]^{1/2}}$$

In the second reaction, the coefficient in front of N<sub>2</sub> is fixed at 1 mole.  $3H_2(g) + N_2(g) \leftrightarrows 2NH_3(g)$  (2)

The reaction quotient for this reaction is  $Q_2 = \frac{\left[NH_3\right]^2}{\left[H_2\right]^3 \left[N_2\right]}$ 

 $Q_2$  is equal to  $Q_1^2$ .

17.12 <u>Plan:</u> Remember that  $Q_c = \frac{\begin{bmatrix} C \end{bmatrix}^r \begin{bmatrix} D \end{bmatrix}^d}{\begin{bmatrix} A \end{bmatrix}^a \begin{bmatrix} B \end{bmatrix}^p}$  where A and B are reactants, C and D are products, and *a*, *b*, *c*, and *d* are

the stoichiometric coefficients in the balanced equation.

Solution:  
a) 4NO(g) + O<sub>2</sub>(g) 
$$\leftrightarrows$$
 2N<sub>2</sub>O<sub>3</sub>(g)  

$$Q_{c} = \frac{\left[N_{2}O_{3}\right]^{2}}{\left[NO\right]^{4}\left[O_{2}\right]}$$
b) SF<sub>6</sub>(g) + 2SO<sub>3</sub>(g)  $\leftrightarrows$  3SO<sub>2</sub>F<sub>2</sub>(g)  

$$Q_{c} = \frac{\left[SO_{2}F_{2}\right]^{3}}{\left[SF_{6}\right]\left[SO_{3}\right]^{2}}$$

c) 
$$2SC1F_5(g) + H_2(g) \leftrightarrows S_2F_{10}(g) + 2HCl(g)$$
  
$$Q_c = \frac{[S_2F_{10}][HC1]^2}{[SCIF_5]^2[H_2]}$$

17.13 a) 
$$2C_{2}H_{6}(g) + 7O_{2}(g) \leftrightarrows 4CO_{2}(g) + 6H_{2}O(g)$$
  

$$Q_{c} = \frac{[CO_{2}]^{4} [H_{2}O]^{6}}{[C_{2}H_{6}]^{2} [O_{2}]^{7}}$$
b)  $CH_{4}(g) + 4F_{2}(g) \leftrightarrows CF_{4}(g) + 4HF(g)$   

$$Q_{c} = \frac{[CF_{4}][HF]^{4}}{[CH_{4}][F_{2}]^{4}}$$
c)  $2SO_{3}(g) \leftrightarrows 2SO_{2}(g) + O_{2}(g)$   

$$Q_{c} = \frac{[SO_{2}]^{2} [O_{2}]}{[SO_{3}]^{2}}$$

17.14 <u>Plan:</u> Remember that  $Q_c = \frac{\begin{bmatrix} C \end{bmatrix}^r \begin{bmatrix} D \end{bmatrix}^d}{\begin{bmatrix} A \end{bmatrix}^a \begin{bmatrix} B \end{bmatrix}^p}$  where A and B are reactants, C and D are products, and *a*, *b*, *c*, and *d* are

the stoichiometric coefficients in the balanced equation.

Solution:  
a) 2NO<sub>2</sub>Cl(g) 
$$\leftrightarrows$$
 2NO<sub>2</sub>(g) + Cl<sub>2</sub>(g)  

$$Q_{c} = \frac{\left[NO_{2}\right]^{2}\left[Cl_{2}\right]}{\left[NO_{2}Cl\right]^{2}}$$
b) 2POCl<sub>3</sub>(g)  $\leftrightarrows$  2PCl<sub>3</sub>(g) + O<sub>2</sub>(g)  

$$Q_{c} = \frac{\left[PCl_{3}\right]^{2}\left[O_{2}\right]}{\left[POCl_{3}\right]^{2}}$$
c) 4NH<sub>3</sub>(g) + 3O<sub>2</sub>(g)  $\leftrightarrows$  2N<sub>2</sub>(g) + 6H<sub>2</sub>O(g)  

$$Q_{c} = \frac{\left[N_{2}\right]^{2}\left[H_{2}O\right]^{6}}{\left[NH_{3}\right]^{4}\left[O_{2}\right]^{3}}$$

17.15 a) 
$$3O_2(g) \leftrightarrows 2O_3(g)$$
  
 $Q_c = \frac{[O_3]^2}{[O_2]^3}$   
b)  $NO(g) + O_3(g) \leftrightarrows NO_2(g) + O_2(g)$   
 $Q_c = \frac{[NO_2][O_2]}{[NO][O_3]}$   
c)  $N_2O(g) + 4H_2(g) \leftrightarrows 2NH_3(g) + H_2O(g)$   
 $Q_c = \frac{[NH_3]^2[H_2O]}{[N_2O][H_2]^4}$ 

17.16 <u>Plan:</u> Compare each equation with the reference equation to see how the direction and coefficients have changed. If a reaction has been reversed, the *K* value is the reciprocal of the *K* value for the reference reaction. If the coefficients have been changed by a factor *n*, the *K* value is equal to the original *K* value raised to the *nth* power.

Solution:

a) The *K* for the original reaction is  $K_c = \frac{[H_2]^2 [S_2]}{[H_2 S]^2}$ 

The given reaction  $1/2S_2(g) + H_2(g) \leftrightarrows H_2S(g)$  is the reverse reaction of the original reaction and the coefficients of the original reaction have been multiplied by a factor of 1/2. The equilibrium constant for the reverse reaction is the reciprocal (1/K) of the original constant. The *K* value of the original reaction is raised to the 1/2 power.

$$K_{c (a)} = (1/K_c)^{1/2} = \frac{\lfloor H_2 S \rfloor}{\lfloor S_2 \rfloor^{1/2} \lfloor H_2 \rfloor}$$
$$K_{c (a)} = (1/1.6 \times 10^{-2})^{1/2} = 7.90569 = 7.9$$

b) The given reaction  $5H_2S(g) \leftrightarrows 5H_2(g) + 5/2S_2(g)$  is the original reaction multiplied by 5/2. Take the original *K* to the 5/2 power to find *K* of given reaction.

$$K_{c (b)} = (K_c)^{5/2} = \frac{\left[H_2\right]^5 \left[S_2\right]^{5/2}}{\left[H_2S\right]^5}$$
$$K_{c (b)} = (1.6x10^{-2})^{5/2} = 3.23817x10^{-5} = 3.2x10^{-5}$$

17.17 
$$K_{c} = \frac{\left[N_{2}\right]\left[H_{2}O\right]^{2}}{\left[NO\right]^{2}\left[H_{2}\right]^{2}}$$
a)  $K_{c (a)} = \left[K_{c}\right]^{1/2} = \frac{\left[N_{2}\right]^{1/2}\left[H_{2}O\right]}{\left[NO\right]\left[H_{2}\right]}$ 
Thus,  $K_{c (a)} = \left[K_{c}\right]^{1/2} = (6.5 \times 10^{2})^{1/2} = 25.495 = 25$ 
b)  $K_{c} = \left[K_{c}\right]^{-2} = \frac{\left[NO\right]^{4}\left[H_{2}\right]^{4}}{\left[N_{2}\right]^{2}\left[H_{2}O\right]^{4}}$ 
 $K_{c} = \left[K_{c}\right]^{-2} = (6.5 \times 10^{2})^{-2} = 2.36686 \times 10^{-6} = 2.4 \times 10^{-6}$ 

17.18 <u>Plan:</u> The concentration of solids and pure liquids do not change, so their concentration terms are not written in the reaction quotient expression. Remember that stoichiometric coefficients are used as exponents in the expression for the reaction quotient. Solution:

a) 
$$2Na_2O_2(s) + 2CO_2(g) \leftrightarrows 2Na_2CO_3(s) + O_2(g)$$
  

$$Q_c = \frac{[O_2]}{[CO_2]^2}$$
b)  $H_2O(l) \leftrightarrows H_2O(g)$   

$$Q_c = [H_2O(g)] \quad \text{Only the gaseous water is used. The "(g)" is for emphasis.}$$
c)  $NH_4Cl(s) \leftrightarrows NH_3(g) + HCl(g)$   

$$Q_c = [NH_3][HCl]$$

17.19 a)  $H_2O(l) + SO_3(g) \leftrightarrows H_2SO_4(aq)$   $Q_c = \frac{[H_2SO_4]}{[SO_3]}$ b) 2KNO<sub>3</sub>(s) \ \ 2KNO\_2(s) + O\_2(g)  $Q_c = [O_2]$ c)  $S_8(s) + 24F_2(g) \leftrightarrows 8SF_6(g)$ 

$$Q_{\rm c} = \frac{\left[\mathrm{SF}_6\right]^8}{\left[\mathrm{F}_2\right]^{24}}$$

17.20 <u>Plan:</u> The concentration of solids and pure liquids do not change, so their concentration terms are not written in the reaction quotient expression. Remember that stoichiometric coefficients are used as exponents in the expression for the reaction quotient.

# Solution:

a) 2NaHCO<sub>3</sub>(s) 
$$\leftrightarrows Na_2CO_3(s) + CO_2(g) + H_2O(g)$$
  
 $Q_c = [CO_2][H_2O]$   
b) SnO<sub>2</sub>(s) + 2H<sub>2</sub>(g)  $\leftrightarrows Sn(s) + 2H_2O(g)$   
 $Q_c = \frac{[H_2O]^2}{[H_2]^2}$   
c) H<sub>2</sub>SO<sub>4</sub>(l) + SO<sub>3</sub>(g)  $\leftrightarrows H_2S_2O_7(l)$   
 $Q_c = \frac{1}{[SO_3]}$ 

17.21 a)  $2\operatorname{Al}(s) + 2\operatorname{NaOH}(aq) + 6\operatorname{H}_2\operatorname{O}(l) \leftrightarrows 2\operatorname{Na}[\operatorname{Al}(\operatorname{OH})_4](aq) + 3\operatorname{H}_2(g)$  $\left[\operatorname{Na}\left[\operatorname{Al}(\operatorname{OH})_4\right]\right]^2 \left[\operatorname{H}_2\right]^3$ 

$$Q_{c} = \frac{\left[ \text{NaOH} \right]^{2}}{\left[ \text{NaOH} \right]^{2}}$$

b)  $CO_2(s) \leftrightarrows CO_2(g)$   $Q_c = [CO_2(g)]$  Only the gaseous carbon dioxide is used. The "(g)" is for emphasis. c)  $2N_2O_5(s) \leftrightarrows 4NO_2(g) + O_2(g)$  $Q_c = [NO_2]^4[O_2]$ 

17.22 Write balanced chemical equations for each reaction, and then write the appropriate equilibrium expression. a)  $4HCl(g) + O_2(g) \leftrightarrows 2Cl_2(g) + 2H_2O(g)$ 

$$Q_{c} = \frac{\left[Cl_{2}\right]^{2} \left[H_{2}O\right]^{2}}{\left[HCI\right]^{4} \left[O_{2}\right]}$$
  
b) 2As<sub>2</sub>O<sub>3</sub>(s) + 10F<sub>2</sub>(g) \(\infty\) 4AsF<sub>5</sub>(l) + 3O<sub>2</sub>(g)  
$$Q_{c} = \frac{\left[O_{2}\right]^{3}}{\left[F_{2}\right]^{10}}$$
  
c) SF<sub>4</sub>(g) + 2H<sub>2</sub>O(l) \(\infty\) SO<sub>2</sub>(g) + 4HF(g)  
$$Q_{c} = \frac{\left[SO_{2}\right]\left[HF\right]^{4}}{\left[SF_{4}\right]}$$
  
d) 2MoO<sub>3</sub>(s) + 6XeF<sub>2</sub>(g) \(\infty\) 2MoF<sub>6</sub>(l) + 6Xe(g) + 3O<sub>2</sub>(g)  
$$Q_{c} = \frac{\left[Xe\right]^{6}\left[O_{2}\right]^{3}}{\left[XeF_{2}\right]^{6}}$$

17.23 <u>Plan:</u> Add the two equations, canceling substances that appear on both sides of the equation. Write the  $Q_c$  expression for each of the steps and for the overall equation. Since the individual steps are added, their  $Q_c$ 's are multiplied and common terms are canceled to obtain the overall  $Q_c$ .

#### Solution:

a) The balanced equations and corresponding reaction quotients are given below. Note the second equation must be multiplied by 2 to get the appropriate overall equation.

-2

(1) 
$$\operatorname{Cl}_{2}(g) + \operatorname{F}_{2}(g) \leftrightarrows \operatorname{2ClF}(g)$$
  

$$Q_{1} = \frac{\left[\operatorname{ClF}\right]}{\left[\operatorname{Cl}_{2}\right]\left[\operatorname{F}_{2}\right]}$$

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]^{2}}{\left[\operatorname{ClF}\right]^{2}\left[\operatorname{F}_{2}\right]^{2}}$$
Overall:  $\operatorname{Cl}_{2}(g) + 3\operatorname{F}_{2}(g) \leftrightarrows 2\operatorname{ClF}_{3}(g)$   

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]^{2}}{\left[\operatorname{ClF}\right]^{2}\left[\operatorname{F}_{2}\right]^{2}}$$

$$Q_{\text{overall}} = \frac{\left[\operatorname{ClF}_{3}\right]^{2}}{\left[\operatorname{Cl}_{2}\right]\left[\operatorname{F}_{2}\right]^{3}}$$

b) The reaction quotient for the overall reaction,  $Q_{\text{overall}}$ , determined from the reaction is:

$$Q_{\text{overall}} = \frac{\left[\text{ClF}_{3}\right]^{2}}{\left[\text{Cl}_{2}\right]\left[\text{F}_{2}\right]^{3}}$$

$$Q_{\text{overall}} = Q_{1}Q_{2}^{2} = \frac{\left[\text{ClF}\right]^{2}}{\left[\text{Cl}_{2}\right]\left[\text{F}_{2}\right]} \times \frac{\left[\text{ClF}_{3}\right]^{2}}{\left[\text{ClF}\right]^{2}\left[\text{F}_{2}\right]^{2}} = \frac{\left[\text{ClF}_{3}\right]^{2}}{\left[\text{Cl}_{2}\right]\left[\text{F}_{2}\right]^{3}}$$

- 17.24 According to the ideal gas equation, PV = nRT. Concentration and pressure of gas are directly proportional as long as the temperature is constant: C = n/V = P/RT.
- 17.25  $K_c$  and  $K_p$  are related by the equation  $K_p = K_c (RT)^{\Delta n}$ , where  $\Delta n$  represents the change in the number of moles of gas in the reaction (moles gaseous products moles gaseous reactants). When  $\Delta n$  is zero (no change in number of moles of gas), the term  $(RT)^{\Delta n}$  equals 1 and  $K_c = K_p$ . When  $\Delta n$  is not zero, meaning that there is a change in the number of moles of gas in the reaction, then  $K_c \neq K_p$ .
- a) K<sub>p</sub> = K<sub>c</sub>(RT)<sup>Δn</sup>. Since Δn = number of moles gaseous products number of moles gaseous reactants, Δn is a positive integer for this reaction. If Δn is a positive integer, then (RT)<sup>Δn</sup> is greater than 1. Thus, K<sub>c</sub> is multiplied by a number that is greater than 1 to give K<sub>p</sub>. K<sub>c</sub> is smaller than K<sub>p</sub>.
  b) Assuming that RT > 1 (which occurs when T > 12.2 K, because 0.0821 (R) x 12.2 = 1), K<sub>p</sub> > K<sub>c</sub> if the number of moles of gaseous products exceeds the number of moles of gaseous reactants. K<sub>p</sub> < K<sub>c</sub> when the number of moles of gaseous reactants exceeds the number of gaseous product.

17.27 <u>Plan:</u>  $\Delta n_{gas} =$  moles gaseous products – moles gaseous reactants. <u>Solution:</u> a) Number of moles of <u>gaseous</u> reactants = 0; number of moles of <u>gaseous</u> products = 3;  $\Delta n_{gas} = 3 - 0 = 3$ b) Number of moles of <u>gaseous</u> reactants = 1; number of moles of <u>gaseous</u> products = 0;  $\Delta n_{gas} = 0 - 1 = -1$ c) Number of moles of <u>gaseous</u> reactants = 0; number of moles of <u>gaseous</u> products = 3;  $\Delta n_{gas} = 3 - 0 = 3$ 

17.28 a) 
$$\Delta n_{gas} = 1$$
 b)  $\Delta n_{gas} = -3$  c)  $\Delta n_{gas} = 1$ 

17.29 <u>Plan:</u> First, determine  $\Delta n$  for the reaction and then calculate  $K_c$  using  $K_p = K_c (RT)^{\Delta n}$ . <u>Solution:</u> a)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 1 – 2 = –1

$$K_{\rm p} = K_{\rm c} (RT)^{\Delta}$$

$$K_{\rm c} = \frac{K_{\rm p}}{(RT)^{\Delta n}} = \frac{3.9 \text{x} 10^{-2}}{[(0.0821)(1000.)]^{-1}} = 3.2019 = 3.2$$

b)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 1 – 1 = 0

$$K_{\rm c} = \frac{K_{\rm p}}{(RT)^{\Delta n}} = \frac{28.5}{\left[(0.0821)(500.)\right]^0} = 28.5$$

17.30 First, determine  $\Delta n$  for the reaction and then calculate  $K_c$  using  $K_p = K_c (RT)^{\Delta n}$ . a)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 2 = 0

$$K_{\rm c} = \frac{K_{\rm p}}{(RT)^{\Delta n}} = \frac{49}{\left[(0.0821)(730.)\right]^0} = 49$$

b)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 3 = –1

$$K_{\rm c} = \frac{K_{\rm p}}{(RT)^{\Delta n}} = \frac{2.5 \times 10^{10}}{\left[(0.0821)(500.)\right]^{-1}} = 1.02625 \times 10^{12} = 1.0 \times 10^{12}$$

17.31 <u>Plan:</u> First, determine  $\Delta n$  for the reaction and then calculate  $K_p$  using  $K_p = K_c (RT)^{\Delta n}$ . Solution:

a)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 1 = 1

- $K_{\rm p} = K_{\rm c} (RT)^{\Delta n} = (6.1 \times 10^{-3}) [(0.0821)(298)]^{1} = 0.14924 = 0.15$ b)  $\Delta n$  = moles gaseous products moles gaseous reactants = 2 4 = -2  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n} = (2.4 \times 10^{-3}) [(0.0821)(1000.)]^{-2} = 3.5606 \times 10^{-7} = 3.6 \times 10^{-7}$
- First, determine  $\Delta n$  for the reaction and then calculate  $K_p$  using  $K_p = K_c (RT)^{\Delta n}$ . 17.32 a)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 2 = 0  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n} = (0.77)[(0.0821)(1020.)]^0 = 0.77$ b)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 3 = –1  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n} = (1.8 \times 10^{-56})[(0.0821)(570.)]^{-1} = 3.8464 \times 10^{-58} = 3.8 \times 10^{-58}$
- 17.33 When Q < K, the reaction proceeds to the **right** to form more products. The reaction quotient and equilibrium constant are determined by [products]/[reactants]. For Q to increase and reach the value of K, the concentration of products (numerator) must increase in relation to the concentration of reactants (denominator).

17.34 a) The reaction is 
$$2D \leftrightarrow E$$
 and  $K_c = \frac{[E]}{[D]^2}$ 

Concentration of D = Concentration of E =  $(3 \text{ spheres}) \left( \frac{0.0100 \text{ mol}}{1 \text{ sphere}} \right) \left( \frac{1}{1.00 \text{ L}} \right) = 0.0300 \text{ M}$ 

$$K_{\rm c} = \frac{[{\rm E}]}{[{\rm D}]^2} = \frac{[0.0300]}{[0.0300]^2} = 33.3333 = 33.3$$

b) In Scene B the concentrations of D and E are both 0.0300 mol/0.500 L = 0.0600 M

$$Q_{\rm c} = \frac{[{\rm E}]}{[{\rm D}]^2} = \frac{[0.0600]}{[0.0600]^2} = 16.666666 = 16.7$$

B is not at equilibrium. Since  $Q_c < K_c$ , the reaction will proceed to the right.

In Scene C, the concentration of D is still 0.0600 M and the concentration of E is 0.0600 mol/0.500 L = 0.120 M LE I [0 120]

$$Q_{\rm c} = \frac{[{\rm L}]}{[{\rm D}]^2} = \frac{[0.120]}{[0.0600]^2} = 33.3333 = 33.3$$

Since  $Q_c = K_c$  in Scene C, the reaction is at equilibrium.

<u>Plan</u>: To decide if the reaction is at equilibrium, calculate  $Q_p$  and compare it to  $K_p$ . If  $Q_p = K_p$ , then the reaction is at equilibrium. If  $Q_p > K_p$ , then the reaction proceeds to the left to produce more reactants. If  $Q_p < K_p$ , then the 17.35 reaction proceeds to the right to produce more products.

Solution:

$$Q_{\rm p} = \frac{{\rm P}_{{\rm H}_2} {\rm P}_{{\rm Br}_2}}{{\rm P}_{{\rm HBr}}^2} = \frac{(0.010)(0.010)}{(0.20)^2} = 2.5 {\rm x} 10^{-3} > K_{\rm p} = 4.18 {\rm x} 10^{-9}$$

 $Q_p > K_p$ , thus, the reaction is **not** at equilibrium and will proceed to the **left** (towards the reactants). Thus, the numerator will decrease in size as products are consumed and the denominator will increase in size as more reactant is produced.  $Q_p$  will decrease until  $Q_p = K_p$ .

17.36 
$$Q_{\rm p} = \frac{P_{\rm NO}^2 P_{\rm Br_2}}{P_{\rm NOBr}^2} = \frac{(0.10)^2 (0.10)}{(0.10)^2} = 0.10 < K_{\rm p} = 60.6$$

 $Q_{p} < K_{p}$  Thus, the reaction is **not** at equilibrium and will proceed to the **right** (towards the products).

17.37 There is insufficient information to calculate the partial pressures of each gas (*T* is not given). There is sufficient information to determine the concentrations and hence  $Q_c$ . Convert the  $K_p$  given to  $K_c$  using  $K_p = K_c (RT)^{\Delta n}$ . Compare the  $Q_c$  to the  $K_c$  just calculated and make a prediction.

 $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 2 = 0 Since  $\Delta n = 0$ ,  $K_p = K_c = 2.7$  (Note: If  $\Delta n$  had any other value, we could not finish the calculation without the temperature.)

$$Q_{\rm c} = \frac{\left[{\rm CO}_2\right]\left[{\rm H}_2\right]}{\left[{\rm CO}\right]\left[{\rm H}_2{\rm O}\right]} = \frac{\left[0.62/2.0\right]\left[0.43/2.0\right]}{\left[0.13/2.0\right]\left[0.56/2.0\right]} = 3.662 > K_{\rm c} = 2.7$$

 $Q_{\rm c} > K_{\rm c}$  Thus, the reaction is **not** at equilibrium and will proceed to the **left** (towards the reactants).

- 17.38 At equilibrium, equal concentrations of  $CFCl_3$  and HCl exist, regardless of starting reactant concentrations. The equilibrium concentrations of  $CFCl_3$  and HCl would still be equal if unequal concentrations of  $CCl_4$  and HF were used. This occurs only when the two products have the same coefficients in the balanced equation. Otherwise, more of the product with the larger coefficient will be produced.
- 17.39 When x mol of  $CH_4$  reacts, 2x mol of  $H_2O$  also reacts to form x mol of  $CO_2$  and 4x mol of  $H_2$ . This is based on the 1:2:1:4 mole ratio in the reaction. The final (equilibrium) concentration of each reactant is the initial concentration minus the amount that reacts. The final (equilibrium) concentration of each product is the initial concentration plus the amount that forms.
- a) The approximation applies when the change in concentration from initial to equilibrium is so small that it is insignificant. This occurs when *K* is small and initial concentration is large.
  b) This approximation will not work when the change in concentration is greater than 5%. This can occur when [reactant]<sub>initial</sub> is very small, or when [reactant]<sub>change</sub> is relatively large due to a large *K*.
- 17.41 <u>Plan:</u> Since all equilibrium concentrations are given in molarities and the reaction is balanced, construct an equilibrium expression and substitute the equilibrium concentrations to find  $K_c$ . <u>Solution:</u>

$$K_{\rm c} = \frac{\left[\mathrm{HI}\right]^2}{\left[\mathrm{H}_2\right]\left[\mathrm{I}_2\right]} = \frac{\left[1.87 \mathrm{x} 10^{-3}\right]^2}{\left[6.50 \mathrm{x} 10^{-5}\right]\left[1.06 \mathrm{x} 10^{-3}\right]} = 50.753 = 50.8$$

17.42 
$$K_{\rm c} = \frac{[N_2][H_2]^3}{[NH_3]^2} = \frac{[0.114][0.342]^3}{[0.0225]^2} = 9.0077875 = 9.01$$

17.43 <u>Plan:</u> Calculate the initial concentration of  $PCl_5$  from the given number of moles and the container volume; the reaction is proceeding to the right, consuming  $PCl_5$  and producing products. There is a 1:1:1 mole ratio between the reactants and products.

Solution:

Initial  $[PCl_5] = 0.15 \text{ mol}/2.0 \text{ L} = 0.075 M$ 

Since there is a 1:1:1 mole ratio in this reaction:

$\mathbf{x} = [PCl_5] \mathbf{r}$	eacting (-x), and th	ne amount c	of $PCl_3$ and of	$Cl_2$ for	ming (+x).
Concentration (M)	$PCl_5(g)$	⇆	$PCl_3(g)$	+	$Cl_2(g)$
Initial	0.075		0		0
Change	-X		+x		$+\mathbf{x}$
Equilibrium	0.075 - x		х		х

17.44 The reaction table requires that the initial  $[H_2]$  and  $[F_2]$  be calculated:  $[H_2] = 0.10 \text{ mol}/0.50 \text{ L} = 0.20 \text{ M}$ ;  $[F_2] = 0.050 \text{ mol}/0.50 \text{ L} = 0.10 M.$ 

$x = [H_2] = [$	F <sub>2</sub> ] reacting (-	x); $2x = [HF]$ for	ming $(+2x)$
Concentration (M)	$H_2(g)$	+ $F_2(g)$	$\Rightarrow$ 2HF(g)
Initial	0.20	0.10	0
Change	-X	-X	+2x
Equilibrium	0.20 - x	0.10 - x	2x

17.45 <u>Plan</u>: Two of the three equilibrium pressures are known, as is  $K_p$ . Construct an equilibrium expression and solve for  $P_{\text{NOCl}}$ . Solution:

$$K_{\rm p} = 6.5 \times 10^4 = \frac{P_{\rm NOCl}^2}{P_{\rm NO}^2 P_{\rm Cl_2}}$$
$$6.5 \times 10^4 = \frac{P_{\rm NOCl}^2}{(0.35)^2 (0.10)}$$

$$P_{\text{NOC1}} = \sqrt{(6.5 \times 10^4)(0.35)^2(0.10)} = 28.2179 = 28 \text{ atm}$$

A high pressure for NOCl is expected because the large value of  $K_p$  indicates that the reaction proceeds largely to the right, i.e., to the formation of products.

17.46 
$$C(s) + 2H_2(g) \leftrightarrows CH_4(g)$$
  
 $K_p = \frac{P_{CH_4}}{P_{H_2}^2} = 0.262$   
 $P_{CH_4} = K_p P_{H_2}^2 = (0.262)(1.22)^2 = 0.38996 = 0.390 \text{ atm}$ 

17.47 Plan: Use the balanced equation to write an equilibrium expression and to define x. Set up a reaction table, substitute into the  $K_p$  expression, and solve for x. Solution:

 $NH_4HS(s) \leftrightarrows H_2S(g) + NH_3(g)$ 

 $x = [NH_4HS]$  reacting (-x), and the amount of  $H_2S$  and of  $NH_3$  forming (+x) since there is a 1:1:1 mole ratio between the reactant and products.

(It is not necessary to calculate the molarity of NH4HS since, as a solid, it is not included in the equilibrium expression.)

Concentration (M)	$NH_4HS(s)$	₽	$H_2S(g)$	+	$NH_3(g)$
Initial			0		0
Change	-X		+x		+x
Equilibrium			Х		Х

$$K_{\rm p} = 0.11 = (P_{\rm H_2S})(P_{\rm NH_3})$$
 (The solid NH<sub>4</sub>HS is not included.)  
 $0.11 = (x)(x)$   
 $x = P_{\rm NH_3} = 0.33166 = 0.33$  atm

17.48  $2H_2S(g) \leftrightarrows 2H_2(g) + S_2(g)$ 

$$\begin{bmatrix} H_2S \end{bmatrix} = 0.45 \text{ mol}/3.0 \text{ L} = 0.15 \text{ M}$$
  
Concentration (M) 2H<sub>2</sub>S(g)  $\rightleftharpoons 2H_2(g) + S_2(g)$   
Initial 0.15 0 0  
Change  $-2x + 2x + x$   
Equilibrium  $0.15 - 2x 2x x$   

$$K_c = 9.30x10^{-8} = \frac{\left[H_2\right]^2 \left[S_2\right]}{\left[H_2S\right]^2} = \frac{\left[2x\right]^2 \left[x\right]}{\left[0.15 - 2x\right]^2}$$
Assuming  $0.15 \text{ M} - 2 \text{ x} \approx 0.15 \text{ M}$   
 $9.30x10^{-8} = \frac{\left[2x\right]^2 \left[x\right]}{\left[0.15\right]^2} = \frac{4x^3}{0.15^2}$   
 $x = 8.0575x10^{-4} \text{ M}$   
 $\left[H_2\right] = 2x = 2 (8.0575x10^{-4} \text{ M}) = 1.6115x10^{-3} = 1.6x10^{-3} \text{ M}$   
(Since  $(1.6x10^{-3})/(0.15) < 0.05$ , the assumption is OK.)

17.49 <u>Plan:</u> Use the balanced equation to write an equilibrium expression. Find the initial concentration of each reactant from the given amounts and container volume, use the balanced equation to define x and set up a reaction table, substitute into the equilibrium expression, and solve for x, from which the concentration of NO is calculated.

Solution:

17.50

The initial concentrations of N<sub>2</sub> and O<sub>2</sub> are (0.20 mol/1.0 L) = 0.20 M and (0.15 mol/1.0 L) = 0.15 M, respectively.

 $N_2(g) + O_2(g) \leftrightarrows 2NO(g)$ There is a 1:1:2 mole ratio between reactants and products.  $N_2(g) +$ Concentration (*M*)  $O_2(g)$ ⇆ 2NO(g)0.20 Initial 0.15 0  $\frac{-x}{0.20 - x}$  $\frac{-x}{0.15 - x}$ +2x(1:1:2 mole ratio) Change 2x Equilibrium  $K_{\rm c} = 4.10 {\rm x} 10^{-4} = \frac{[{\rm NO}]^2}{[{\rm N}_2][{\rm O}_2]} = \frac{[2 {\rm x}]^2}{[0.20 - {\rm x}][0.15 - {\rm x}]}$ Assume  $0.20 M - x \approx 0.20 M$  $0.15 M - x \approx 0.15 M$ and  $4.10 \mathrm{x} 10^{-4} = \frac{4 \mathrm{x}^2}{[0.20][0.15]}$  $x = 1.753568 \times 10^{-3} M$  $[NO] = 2x = 2(1.753568x10^{-3} M) = 3.507136x10^{-3} = 3.5x10^{-3} M$  $(\text{Since } (1.8 \times 10^{-3})/(0.15) < 0.05$ , the assumption is OK.)  $2NO_2(g) \leftrightarrows 2NO(g) + O_2(g)$ Pressure (atm)  $2NO_2(g)$ 2NO(g) $O_2(g)$ -2x0.75 - 2x 0 Initial 0 +2x Change +xEquilibrium  $K_{\rm p} = 4.48 \mathrm{x} 10^{-13} = \frac{P_{\rm NO}^2 P_{\rm O_2}}{P_{\rm NO_2}^2} = \frac{(2 \mathrm{x})^2 (\mathrm{x})}{(0.75 - 2 \mathrm{x})^2}$ 

Assume 0.75 atm - 2x 
$$\approx$$
 0.75 atm  
4.48x10<sup>-13</sup> =  $\frac{(4x^2)(x)}{(0.75)^2} = \frac{(4x^3)}{(0.75)^2}$   
x = 3.979x10<sup>-5</sup> atm = **4.0x10<sup>-5</sup> atm O**<sub>2</sub>

$$P_{\rm NO} = 2x = 2(3.979 \times 10^{-5} \text{ atm}) = 7.958 \times 10^{-5} = 8.0 \times 10^{-5} \text{ atm NO}$$

17.51 <u>Plan:</u> Find the initial concentration of each reactant and product from the given amounts and container volume, use the balanced equation to define x, and set up a reaction table. The equilibrium concentration of  $H_2$  is known, so x can be calculated and used to find the other equilibrium concentrations.

Solution:

Initial concentrations:

[HI] = (0.0244 mol)/(1.50 L) = 0.0162667 M $[H_2] = (0.00623 \text{ mol})/(1.50 \text{ L}) = 0.0041533 M$  $[I_2] = (0.00414 \text{ mol})/(1.50 \text{ L}) = 0.00276 M$  $2 \operatorname{HI}(g) \leftrightarrows$  $H_2(g) + I_2(g)$ There is a 2:1:1 mole ratio between reactants and products. Concentration (M)2 HI(g)⇆  $H_2(g)$ + $I_2(g)$ Initial 0.0162667 0.0041533 0.00276 2:1:1 mole ratio Change -2x +x+xEquilibrium 0.0162667 - 2x0.0041533 + x0.00276 + x $[H_2]_{eq} = 0.00467 = 0.0041533 + x$ x = 0.0005167 M $[I_2]_{eq} = 0.00276 + x = 0.00276 + 0.0005167 = 0.0032767 = \textbf{0.00328} \ \textbf{M} \ \textbf{I_2}$  $[\text{HI}]_{\text{eq}} = 0.0162667 - 2x = 0.0162667 - 2(0.0005167) = 0.0152333 = 0.0152 M \text{ HI}$ 

17.52 Initial concentrations:

 $[A] = (1.75 \times 10^{-3} \text{ mol})/(1.00 \text{ L}) = 1.75 \times 10^{-3} M$   $[B] = (1.25 \times 10^{-3} \text{ mol})/(1.00 \text{ L}) = 1.25 \times 10^{-3} M$   $[C] = (6.50 \times 10^{-4} \text{ mol})/(1.00 \text{ L}) = 6.50 \times 10^{-4} M$ Concentration (M)A(g)⇇ 2B(g) $1.75 \times 10^{-3}$  $1.25 \times 10^{-3}$  $6.50 \times 10^{-4}$ Initial Change - x  $1.75 \times 10^{-3} - x$ Equilibrium  $[A]_{eq} = 2.15 \times 10^{-3} = 1.75 \times 10^{-3} - x$ x = -0.00040 $[B]_{eq} = 1.25 \times 10^{-3} + 2x = 4.5 \times 10^{-4} M$  $[C]_{eq} = 6.50 \times 10^{-4} + x = 2.5 \times 10^{-4} M$ 

17.53 <u>Plan:</u> Use the balanced equation to write an equilibrium expression. Find the initial concentration of ICl from the given amount and container volume, use the balanced equation to define x and set up a reaction table, substitute into the equilibrium expression, and solve for x, from which the equilibrium concentrations can be calculated.

Solution:  $[IC1]_{init} = (0.500 \text{ mol}/5.00 \text{ L}) = 0.100 M$ Concentration (*M*) ⇆ 2ICl(g) $Cl_2(g)$  $I_2(g)$ Initial 0.100 0 0 Change -2x(2:1:1 mole ratio) +x Equilibrium 0.100 - 2xХ  $K_{\rm c} = 0.110 = \frac{[I_2][Cl_2]}{[ICl]^2} = \frac{[x][x]}{[0.100 - 2x]^2}$  $0.110 = \frac{\left[x\right]^2}{\left[0.100 - 2\,x\right]^2}$ Take the square root of each side:  $0.331662 = \frac{[x]}{[0.100 - 2x]}$ x = 0.0331662 - 0.663324x1.663324x = 0.0331662

- 17.54 Concentration (M) $SCl_2(g)$  $2C_{2}H_{4}(g)$  $S(CH_2CH_2Cl)_2(g)$ Initial 0.675 0.973 0 Change 2x+x0.675 - xEquilibrium 0.973 - 2xХ  $[S(CH_2CH_2Cl)_2]_{eq} = x = 0.350 M$  $[SCl_2]_{eq} = 0.675 - x = 0.675 - 0.350 = 0.325 M$  $[C_2H_4]_{eq} = 0.973 - 2x = 0.973 - 2(0.350) = 0.273 M$  $K_{\rm c} = \frac{\left[\mathrm{S}(\mathrm{CH}_{2}\mathrm{CH}_{2}\mathrm{Cl})_{2}\right]}{\left[\mathrm{S}\mathrm{Cl}_{2}\right]\left[\mathrm{C}_{2}\mathrm{H}_{4}\right]^{2}} = \frac{\left[0.350\right]}{\left[0.325\right]\left[0.273\right]^{2}} = 14.4497$  $K_{\rm p} = K_{\rm c}(RT)^{\Delta n}$   $\Delta n = 1 \text{ mol} - 3 \text{ mol} = -2$  $K_{\rm p} = (14.4497) [(0.0821)(273.2 + 20.0)]^{-2} = 0.0249370 = 0.0249$
- 17.55 <u>Plan</u>: Use the balanced equation to write an equilibrium expression. Find the initial concentration of each reactant from the given amounts and container volume, use the balanced equation to define x, and set up a reaction table. The equilibrium concentration of  $N_2$  is known, so x can be calculated and used to find the other equilibrium concentrations. Substitute the equilibrium concentrations into the equilibrium expression to find  $K_c$ . <u>Solution</u>:
- $4NH_3(g) + 3O_2(g) \leftrightarrows 2N_2(g) + 6H_2O(g)$ Initial  $[NH_3] = Initial [O_2] = (0.0150 \text{ mol})/(1.00 \text{ L}) = 0.0150 \text{ M}$ Concentration (*M*)  $4NH_3(g)$  $6H_2O(g)$ + $3O_2(g)$  $2N_2(g)$ 0.0150 Initial 0.0150 0 0 Change +2x+6x-4x -3x 0.0150 - 4 Equilibrium 0.0150 - 3x+2x+6x $[N_2]_{eq} = 2x = 1.96 \times 10^{-3} M$ x = (1.96x10<sup>-3</sup> M)/2 = 9.80x10<sup>-4</sup> M  $[H_2O]_{eq} = 6x = 6(9.80 \times 10^{-4}) = 5.8800 \times 10^{-3} M$  $[NH_3]_{eq} = 0.0150 - 4x = 0.0150 - 4(9.80x10^{-4}) = 1.1080x10^{-2} M$  $[O_2]_{eq} = 0.0150 - 3x = 0.0150 - 3(9.80x10^{-4}) = 1.2060x10^{-2} M$  $K_{\rm c} = \frac{\left[N_2\right]^2 \left[H_2 O\right]^6}{\left[NH_3\right]^4 \left[O_2\right]^3} = \frac{\left[1.96 \times 10^{-3}\right]^2 \left[5.8800 \times 10^{-3}\right]^6}{\left[1.1080 \times 10^{-2}\right]^4 \left[1.2060 \times 10^{-2}\right]^3} = 6.005859 \times 10^{-6} = 6.01 \times 10^{-6}$ 17.56 Pressure (atm) FeO(s) +CO(g)⇆  $CO_2(g)$ Fe(s)+Initial 1.00 0 Change -X +x1.00 - xEquilibrium  $K_{\rm p} = \frac{P_{\rm CO_2}}{P_{\rm CO}} = 0.403 = \frac{\rm x}{1.00 - \rm x}$ x = 0.28724 = 0.287 atm CO<sub>2</sub>

1.00 - x = 1.00 - 0.28724 = 0.71276 = 0.71 atm CO

- 17.57 A change in equilibrium conditions such as a change in concentration of a component, a change in pressure (volume), or a change in temperature.
- 17.58 Equilibrium position refers to the specific concentrations or pressures of reactants and products that exist

at equilibrium, whereas equilibrium constant refers to the overall ratio of equilibrium concentrations and not to specific concentrations. Changes in reactant concentration cause changes in the specific equilibrium concentrations of reactants and products (equilibrium position), but not in the equilibrium constant.

17.59 A positive  $\Delta H_{rxn}$  indicates that the reaction is endothermic, and that heat is consumed in the reaction: NH<sub>4</sub>Cl(s) + heat  $\Rightarrow$  NH<sub>3</sub>(g) + HCl(g)

a) The addition of heat (high temperature) causes the reaction to proceed to the right to counterbalance the effect of the added heat. Therefore, more products form at a higher temperature and container (**B**) with the largest number of product molecules best represents the mixture.

b) When heat is removed (low temperature), the reaction shifts to the left to produce heat to offset that disturbance. Therefore,  $NH_3$  and HCl molecules combine to form more reactant and container (A) with the smallest number of product gas molecules best represents the mixture.

- 17.60 Equilibrium component concentration values may change but the mass action expression of these concentrations is a constant as long as temperature remains constant. Changes in component amounts, pressures (volumes), or addition of a catalyst will not change the value of the equilibrium constant.
- 17.61 a) Rate<sub>f</sub> =  $k_f$ [reactants]<sup>x</sup>. An increase in reactant concentration shifts the equilibrium to the right by increasing the initial forward rate. Since  $K_{eq} = k_f/k_r$  and  $k_f$  and  $k_r$  are not changed by changes in concentration,  $K_{eq}$  remains constant.

b) A decrease in volume causes an increase in concentrations of gases. The reaction rate for the formation of fewer moles of gases is increased to a greater extent. Again, the  $k_f$  and  $k_r$  values are unchanged. c) An increase in temperature increases  $k_r$  to a greater extent for an exothermic reaction and thus lowers the  $K_{eq}$  value.

d) An endothermic reaction can be written as: reactants + heat  $\leftrightarrows$  products. A rise in temperature (increase in heat) favors the forward direction of the reaction, i.e., the formation of products and consumption of reactants. Since K = [products]/[reactants], the addition of heat increases the numerator and decreases the denominator, making  $K_2$  larger than  $K_1$ .

- 17.62  $XY(s) \leftrightarrows X(g) + Y(s)$  Since product Y is a solid substance, addition of solid Y has no effect on the equilibrium position (as long as some Y is present). Scene A best represents the system at equilibrium after the addition of two formula units of Y. More Y is present but the amounts of X and XY do not change.
- 17.63 <u>Plan:</u> If the concentration of a substance in the reaction increases, the equilibrium position will shift to consume some of it. If the concentration of a substance in the reaction decreases, the equilibrium position will shift to produce more of it.

Solution:

a) Equilibrium position shifts **towards products**. Adding a reactant (CO) causes production of more products as the system will act to reduce the increase in reactant by proceeding toward the product side, thereby consuming additional CO.

b) Equilibrium position shifts **towards products**. Removing a product  $(CO_2)$  causes production of more products as the system acts to replace the removed product.

c) Equilibrium position **does not shift**. The amount of a solid reactant or product does not impact the equilibrium as long as there is some solid present.

d) Equilibrium position shifts **towards reactants**. When product is added, the system will act to reduce the increase in product by proceeding toward the reactant side, thereby consuming additional  $CO_2$ ; dry ice is solid carbon dioxide that sublimes to carbon dioxide gas. At very low temperatures,  $CO_2$  solid will not sublime, but since the reaction lists carbon dioxide as a gas, the assumption that sublimation takes place is reasonable.

17.64a) no changeb) no changec) shifts towards the productsd) shifts towards the reactants

17.65 <u>Plan:</u> An increase in container volume results in a decrease in pressure (Boyle's law). Le Châtelier's principle states that the equilibrium will shift in the direction that forms more moles of gas to offset the decrease in pressure.

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Solution:
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a) More F forms (two moles of gas) and less  $F_2$  (one mole of gas) is present as the reaction shifts towards the right.

b) More  $C_2H_2$  and  $H_2$  form (four moles of gas) and less  $CH_4$  (two moles of gas) is present as the reaction shifts towards the right.

a) less CH<sub>3</sub>OH(*l*); more CH<sub>3</sub>OH(*g*)
b) less CH<sub>4</sub> and NH<sub>3</sub>; more HCN and H<sub>2</sub>

17.67 <u>Plan:</u> Decreasing container volume increases the pressure (Boyle's law). Le Châtelier's principle states that the equilibrium will shift in the direction that forms fewer moles of gas to offset the increase in pressure. Solution:

a) There are two moles of reactant gas ( $H_2$  and  $Cl_2$ ) and two moles of product gas (HCl). Since there is the same number of reactant and product gas moles, there is **no effect** on the amounts of reactants or products. b) There are three moles of reactant gases ( $H_2$  and  $O_2$ ) and zero moles of product gas. The reaction will shift to

the

right to produce fewer moles of gas to offset the increase in pressure.  $H_2$  and  $O_2$  will decrease from their initial values before the volume was changed. More  $H_2O$  will form because of the shift in equilibrium position.

# a) more CO<sub>2</sub> and H<sub>2</sub>O; less C<sub>3</sub>H<sub>8</sub> and O<sub>2</sub> b) more NH<sub>3</sub> and O<sub>2</sub>; less N<sub>2</sub> and H<sub>2</sub>O

17.69 <u>Plan:</u> The purpose of adjusting the volume is to cause a shift in equilibrium to the right for increased product yield. Increasing the volume of the container results in a shift in the direction that forms more moles of gas, while decreasing the container volume results in a shift in the direction that forms fewer moles of gas. <u>Solution:</u>

a) Because the number of reactant gaseous moles  $(4H_2)$  equals the product gaseous moles  $(4H_2O)$ , a change in volume will have **no effect** on the yield.

b) The moles of gaseous product (2CO) exceed the moles of gaseous reactant ( $1O_2$ ). A decrease in pressure favors the reaction direction that forms more moles of gas, so **increase** the reaction vessel volume.

# 17.70 a) increase volume b) decrease volume

17.71 <u>Plan:</u> An increase in temperature (addition of heat) causes a shift in the equilibrium <u>away</u> from the side of the reaction with heat. Recall that a negative value of  $\Delta H_{rxn}^{\circ}$  indicates an exothermic reaction, while a positive

value of  $\Delta H_{rxn}^{\circ}$  indicates an endothermic reaction.

Solution:

a)  $CO(g) + 2H_2(g) \leftrightarrows CH_3OH(g) + heat \qquad \Delta H_{rxn}^{\circ} = -90.7 \text{ kJ}$ 

The reaction is exothermic, so heat is written as a product. The equilibrium shifts to the left, away from heat, towards the reactants, so amount of product **decreases**.

b)  $C(s) + H_2O(g) + heat \leftrightarrows CO(g) + H_2(g) \qquad \Delta H_{rxn}^{\circ} = 131 \text{ kJ}$ 

The reaction is endothermic, so heat is written as a reactant. The equilibrium shifts to the right, away from heat, towards the products, so amounts of products **increase**.

c)  $2NO_2(g)$  + heat  $\Rightarrow 2NO(g) + O_2(g)$ 

The reaction is endothermic, so heat is written as a reactant. The equilibrium shifts to the right, away from heat, towards the product, so amounts of products **increase**.

d)  $2C(s) + O_2(g) \leftrightarrows 2CO(g) + heat$ 

The reaction is exothermic, so heat is written as a product. The equilibrium shifts to the left, away from heat, towards the reactants; amount of product **decreases**.

17.72 a) decrease b) decrease c) decrease d) increase

17.73 Plan: The van't Hoff equation shows how the equilibrium constant is affected by a change in temperature. Substitute the given variables into the equation and solve for  $K_2$ . Convert  $\Delta H_{rxn}^{\circ}$  from units of kJ/mol DH to units of J/2 mol DH. Solution:

$$\frac{L}{K_{298}} = K_1 = 1.80 \qquad T_1 = 298 \text{ K}$$

$$K_{500} = K_2 = ? \qquad T_2 = 500. \text{ K} \qquad R = 8.314 \text{ J/mol} \cdot \text{K}$$

$$\Delta H_{rxn}^{\circ} = \left(\frac{0.32 \text{ kJ}}{1 \text{ mol DH}}\right) (2 \text{ mol DH}) \left(\frac{10^3 \text{ J}}{1 \text{ kJ}}\right) = 6.4 \text{ x} 10^2 \text{ J}$$

$$\ln \frac{K_2}{K_1} = -\frac{\Delta H_{rxn}^{\circ}}{R} \left(\frac{1}{T_2} - \frac{1}{T_1}\right)$$

$$\ln \frac{K_2}{1.80} = -\frac{6.4 \text{ x} 10^2 \text{ J}}{8.314 \text{ J/mol} \cdot \text{K}} \left(\frac{1}{500. \text{ K}} - \frac{1}{298 \text{ K}}\right)$$

$$\ln \frac{K_2}{1.80} = 0.104360$$

$$\frac{K_2}{1.80} = 1.110$$

$$K_2 = (1.80)(1.110) = 1.998 = 2.0$$

17.74 The van't Hoff equation shows how the equilibrium constant is affected by a change in temperature. Substitute the given variables into the equation and solve for  $K_2$ .

$$K_{298} = K_1 = 2.25 \times 10^4 \qquad T_1 = 298 \text{ K} \qquad \Delta H_{rxn}^{\circ} = -128 \text{ kJ/mol} \\ K_0 = K_2 = ? \qquad T_2 = (273 + 0.) = 273 \text{ K} \qquad R = 8.314 \text{ J/mol} \cdot \text{K} \\ \Delta H_{rxn}^{\circ} = (-128 \text{ kJ/mol})(10^3 \text{ J/1 kJ}) = -1.28 \times 10^5 \text{ J} \\ \ln \frac{K_2}{K_1} = -\frac{\Delta H_{rxn}^{\circ}}{R} \left(\frac{1}{T_2} - \frac{1}{T_1}\right) \\ \ln \frac{K_2}{2.25 \times 10^4} = -\frac{-1.28 \times 10^5 \text{ J}}{8.314 \text{ J/mol} \cdot \text{K}} \left(\frac{1}{273 \text{ K}} - \frac{1}{298 \text{ K}}\right) \\ \ln \frac{K_2}{2.25 \times 10^4} = 4.731088 \\ \frac{K_2}{2.25 \times 10^4} = 1.134189 \times 10^2 \\ K_2 = (2.25 \times 10^4)(1.134189 \times 10^2) = 2.551925 \times 10^6 = 2.55 \times 10^6 \\ 4\text{Fe}_3\text{O}_4(s) + \text{O}_2(g) \leftrightarrows 6\text{Fe}_2\text{O}_3(s) \qquad K_p = 2.5 \times 10^{87} \text{ at } 298 \text{ K} \\ a) K_p = \frac{1}{P_{O_2}} = 2.5 \times 10^{87} \\ P_{O_2} = 4.0 \times 10^{-88} \text{ atm} \\ b) Q_p = \frac{1}{P_{O_2}} = 1/(0.21) = 4.7619 \\ K_p > Q_p \text{ thus, the reaction will proceed to the right.$$

c)  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$   $K_{\rm c} = K_{\rm p} / (RT)^{\Delta n}$   $K_{\rm c} = (2.5 \times 10^{87}) / [(0.0821)(298)]^{-1} = 6.11645 \times 10^{88} = 6.1 \times 10^{88}$ 

17.75

b)

17.76 Plan: An increase in temperature (addition of heat) causes a shift in the equilibrium away from the side of the reaction with heat, while a decrease in temperature (removal of heat) causes a shift in the equilibrium towards the side with heat. Increasing the volume of the container (pressure decreases) results in a shift in the direction that forms more moles of gas, while decreasing the container volume (pressure increases) results in a shift in the direction that forms fewer moles of gas. Adding a reactant causes a shift in the direction of products.

Solution: a)  $SO_2(g) + 1/2O_2(g) \leftrightarrows SO_3(g) + heat$ 

The forward reaction is exothermic ( $\Delta H_{rxn}^{\circ}$  is negative), so it is favored by **lower temperatures**. Lower temperatures will cause a shift to the right, the heat side of the reaction. There are fewer moles of gas as products (1SO<sub>3</sub>) than as reactants (1SO<sub>2</sub>(g) + 1/2O<sub>2</sub>), so products are favored by **higher pressure**. High pressure will cause a shift in equilibrium to the side with the fewer moles of gas.

b) Addition of O<sub>2</sub> would **decrease** Q since  $Q = \frac{[SO_3]}{[SO_2][O_2]^{1/2}}$ , and have **no impact on** K.

c) To enhance yield of  $SO_3$ , a low temperature is used. Reaction rates are slower at lower temperatures, so a catalyst is used **to speed up the reaction**.

17.77 
$$3H_2(g) + N_2(g) \rightleftharpoons 2NH_3(g)$$
  
 $P_{NH_3} = (41.49\%/100\%)(110. atm) = 45.639 atm$   
 $100.00\% - 41.49\% = 58.51\% N_2 + H_2$   
 $P_{H_2} + P_{N_2} = (58.51\%/100\%)(110. atm) = 64.361 atm$   
 $P_{H_2} = (3/4)(64.361 atm) = 48.27075 atm$   
 $P_{N_2} = (1/4)(64.361 atm) = 16.09025 atm$   
 $K_p = \frac{\left(P_{NH_3}\right)^2}{\left(P_{H_2}\right)^3 \left(P_{N_2}\right)} = \frac{\left(45.639\right)^2}{\left(48.27075\right)^3 \left(16.09025\right)} = 1.15095 \times 10^{-3} = 1.15 \times 10^{-3}$ 

17.78 a)  $3H_2(g) + N_2(g) \rightleftharpoons 2NH_3(g)$  The mole ratio  $H_2:N_2 = 3:1$ ; at equilibrium, if  $N_2 = x$ ,  $H_2 = 3x$ ;  $P_{NH_3} = 50$ . atm

$$K_{\rm p} = \frac{\left(P_{\rm NH_3}\right)^2}{\left(P_{\rm N_2}\right)\left(P_{\rm H_2}\right)^3} = 1.00 \times 10^{-4}$$

$$K_{\rm p} = \frac{\left(50\right)^2}{\left(x\right)\left(3x\right)^3} = 1.00 \times 10^{-4}$$

$$x = 31.02016 = 31 \text{ atm } N_2$$

$$3x = 3(31.02016) = 93.06049 = 93 \text{ atm } H_2$$

$$P_{\rm total} = P_{\rm nitrogen} + P_{\rm hydrogen} + P_{\rm ammonia} = (31.02016 \text{ atm}) + (93.06049 \text{ atm}) + (50. \text{ atm})$$

$$= 174.08065 = 174 \text{ atm total}$$

b) The mole ratio  $H_2:N_2 = 6:1$ ; at equilibrium, if  $N_2 = x$ ,  $H_2 = 6x$ ;  $P_{NH_3} = 50$ . atm

$$K_{\rm p} = \frac{(50.)^2}{(x)(6x)^3} = 1.00x10^{-4}$$
  
x = 18.445 = **18 atm N<sub>2</sub>**  
6x = 6(18.445) = 110.67 = **111 atm H<sub>2</sub>**  
P<sub>total</sub> = P<sub>nitrogen</sub> + P<sub>hydrogen</sub> + P<sub>ammonia</sub> = (18.445 atm) + (110.67 atm) + (50. atm)  
= 179.115 = **179 atm total**

This is not a valid argument. The total pressure in b) is greater than in a) to produce the same amount of NH<sub>3</sub>.

17.79 a) **More CaCO<sub>3</sub>**. Because the forward reaction is exothermic, decreasing the temperature will cause an increase in the amount of CaCO<sub>3</sub> formed as the reaction shifts to the right to produce more heat.

b) Less CaCO<sub>3</sub>. The only gas in the equation is a reactant. Increasing the volume (decreasing the pressure) will cause the equilibrium to shift toward the reactant side and the amount of  $CaCO_3$  formed decreases. c) More CaCO<sub>3</sub>. Increasing the partial pressure of  $CO_2$  will cause more CaCO<sub>3</sub> to be formed as the reaction shifts to the right to consume the added CO<sub>2</sub>.

d) No change. Removing half of the initial CaCO<sub>3</sub> will have no effect on the amount of CaCO<sub>3</sub> formed, because  $CaCO_3$  is a solid.

17.80 a) 
$$Q_{\rm c} = \frac{\left[XY\right]^2}{\left[X_2\right]\left[Y_2\right]}$$

b) Scene A: 
$$Q_c = \frac{[0]^2}{[0.4][0.4]} = \mathbf{0}$$
  
Scene B:  $Q_c = \frac{[0.4]^2}{[0.2][0.2]} = \mathbf{4}$   
Scenes C-E:  $Q_c = \frac{[0.6]^2}{[0.1][0.1]} = 36 = \mathbf{4x10^1}$ 

c) Time is progressing to the **right**. Frame A must be the earliest time.

d)  $K = 4x10^{1}$ 

e) Scene B. At higher temperatures, the reaction shifts to the left (forming more  $X_2$  and  $Y_2$ ).

f) None. Volume (pressure) has no effect on the position of the equilibrium since there are two moles of gas on each side.

17.81 Plan: Use the balanced equation to write an equilibrium expression and to define x. Set up a reaction table, substitute into the  $K_c$  expression, and solve for x. Once the total concentration of the gases at equilibrium is known, the pressure can be found with PV = nRT. Solution

Concentration $(M)$	$NH_2COONH_4(s)$	与	$2NH_3(g)$	+	$CO_2(g)$
Initial	7.80 g		0		0
Change	_		+2x		+x
Equilibrium			2x		х

The solid is irrelevant (as long as some is present) and is not included in the  $K_c$  expression.  $K_{\rm c} = [\rm NH_3]^2 [\rm CO_2]$  $K_{\rm c} = 1.58 \times 10^{-8} = (2 {\rm x})^2 ({\rm x})$ x = 1.580759x10<sup>-3</sup> M

Total concentration of gases =  $2x + x = 2(1.580759x10^{-3} M) + 1.580759x10^{-3} M = 4.742277x10^{-3} M$ To find total pressure use the ideal gas equation: PV = nRT

$$P = \frac{nRT}{V} = \left(\frac{n}{V}\right)RT = MRT$$
  
P = (4.742277x10<sup>-3</sup> M)(0.0821 L•atm/mol•K)(273 + 250.)K = 0.203625 = **0.204 atm**

17.82

a)

(1)  $2Ni_3S_2(s) + 7O_2(g) \leftrightarrows \frac{6NiO(s)}{2} + 4SO_2(g)$ 

 $6NiO(s) + 6H_2(g) \leftrightarrows 6Ni(s) + 6H_2O(g)$ (2)

 $6Ni(s) + 24CO(g) \leftrightarrows 6Ni(CO)_4(g)$ (3)

Overall:  $2Ni_3S_2(s) + 7O_2(g) + 6H_2(g) + 24CO(g) \Rightarrow 4\overline{SO_2(g)} + 6H_2O(g) + 6Ni(CO)_4(g)$ b) As always, the solid is not included in the Q expression.

$$Q_{c(overall)} = \frac{\left[SO_{2}\right]^{4} \left[H_{2}O\right]^{6} \left[Ni(CO)_{4}\right]^{6}}{\left[O_{2}\right]^{7} \left[H_{2}\right]^{6} \left[CO\right]^{24}}$$

$$Q_{1} \times Q_{2} \times Q_{3} = \frac{\left[SO_{2}\right]^{4}}{\left[O_{2}\right]^{7}} \times \frac{\left[H_{2}O\right]^{6}}{\left[H_{2}\right]^{6}} \times \frac{\left[Ni(CO)_{4}\right]^{6}}{\left[CO\right]^{24}} = \frac{\left[SO_{2}\right]^{4} \left[H_{2}O\right]^{6} \left[Ni(CO)_{4}\right]^{6}}{\left[O_{2}\right]^{7} \left[H_{2}\right]^{6} \left[CO\right]^{24}}$$

17.83 a) Since the volume is 1.00 L, the molarity equals the number of moles present.

$$\begin{aligned} & 2\mathrm{NH}_{3}(g) & \leftrightarrows & \mathrm{N}_{2}(g) + 3\mathrm{H}_{2}(g) \\ & \mathrm{Initial} & 0 & 1.30 & 1.65 \\ & \underline{\mathrm{Change}} & +2x & -x & -3x \\ & \mathrm{Equilibrium} & 2x = 0.100 \, M & 1.30 - x & 1.65 - 3x \\ & \mathrm{x} = 0.0500 \, \mathrm{mol} \\ & [\mathrm{N}_{2}]_{eq} = (1.30 - 0.0500) \, M = \mathbf{1.25} \, M \, \mathrm{N}_{2} \\ & [\mathrm{H}_{2}]_{eq} = [1.65 - 3(0.0500)] \, M = \mathbf{1.50} \, M \, \mathrm{H}_{2} \\ & K_{c} = \frac{\left[\mathrm{N}_{2}\right]\left[\mathrm{H}_{2}\right]^{3}}{\left[\mathrm{NH}_{3}\right]^{2}} = \frac{\left[1.25\right]\left[1.50\right]^{3}}{\left[0.100\right]^{2}} = 421.875 = \mathbf{422} \\ & \mathrm{b}) \, K_{c} = \frac{\left[\mathrm{N}_{2}\right]^{\frac{1}{2}}\left[\mathrm{H}_{2}\right]^{\frac{3}{2}}}{\left[\mathrm{NH}_{3}\right]} = \frac{\left[1.50\right]^{\frac{1}{2}}\left[1.25\right]^{\frac{3}{2}}}{\left[8.34\mathrm{x10}^{-2}\right]} = 20.523177 = \mathbf{20.5} \end{aligned}$$

c)  $K_c$  in a) is the square of  $K_c$  in b). The balanced equations are different; therefore, the values of  $K_c$  are different.

- 17.84 <u>Plan:</u> Write the equilibrium expression. You are given a value of  $K_c$  but the amounts of reactant and product are given in units of pressure. Convert  $K_c$  to  $K_p$  and use the equilibrium pressures of  $C_2H_5OH$  and  $H_2O$  to obtain the equilibrium pressure of  $C_2H_4$ . An increase in temperature (addition of heat) causes a shift in the equilibrium away from the side of the reaction with heat, while a decrease in temperature (removal of heat) causes a shift in the equilibrium towards the side with heat. Increasing the volume of the container (pressure decreases) results in a shift in the direction that forms more moles of gas, while decreasing the container volume (pressure increases) results in a shift in the direction that forms fewer moles of gas. The van't Hoff equation shows how the equilibrium constant is affected by a change in temperature. Substitute the given variables into the equation and solve for *K* at 450. K.
  - Solution:
  - a)  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$

 $\Delta n$  = moles gaseous products – moles gaseous reactants = 1 – 2 = –1 (one mol of product, C<sub>2</sub>H<sub>5</sub>OH, and two mol of reactants, C<sub>2</sub>H<sub>4</sub> + H<sub>2</sub>O)

 $K_{\rm p} = K_{\rm c} (RT)^{-1} = (9 \times 10^3) [(0.0821 \text{ L} \cdot \text{atm/mol} \cdot \text{K})(600. \text{ K})]^{-1} = 1.82704 \times 10^2$ 

Substitute the given values into the equilibrium expression and solve for  $P_{C_2H_4}$ .

$$K_{\rm p} = \frac{P_{\rm C_2H_5OH}}{P_{\rm C_2H_4}P_{\rm H_2O}} = \frac{200.}{P_{\rm C_2H_4}(400.)} = 1.8270 \times 10^2$$
$$P_{\rm C_2H_4} = 2.7367 \times 10^{-3} = 3 \times 10^{-3} \text{ atm}$$

b) Since  $\Delta H_{rxn}^{\circ}$  is negative, the reaction is exothermic and heat is written as a product. To shift the reaction towards the right to yield more ethanol, heat must be removed. A **low temperature** favors an exothermic reaction. The forward direction, towards the production of ethanol, produces the smaller number of moles of gas and is favored by **high pressure**.

c) 
$$K_1 = 9x10^3$$
  $T_1 = 600. \text{ K}$   $\Delta H_{rxn}^\circ = (-47.8 \text{ kJ}) \left(\frac{10^3 \text{ J}}{1 \text{ kJ}}\right) = -4.78x10^4 \text{ J}$   
 $K_2 = ?$   $T_2 = 450. \text{ K}$   $R = 8.314 \text{ J/mol} \cdot \text{K}$   
 $\ln \frac{K_2}{K_1} = -\frac{\Delta H_{rxn}^\circ}{R} \left(\frac{1}{T_2} - \frac{1}{T_1}\right)$   
 $\ln \frac{K_2}{9x10^3} = -\frac{-4.78x10^4 \text{ J}}{8.314 \text{ J/mol} \cdot \text{K}} \left(\frac{1}{450. \text{ K}} - \frac{1}{600. \text{ K}}\right)$   
 $\ln \frac{K_2}{9x10^3} = 3.1940769$ 

$$\frac{K_2}{9x10^3} = 24.38765$$
  

$$K_2 = (9x10^3)(24.38765) = 2.1949x10^5 = 2x10^5$$

d) No, condensing the  $C_2H_5OH$  would not increase the yield. Ethanol has a lower boiling point (78.5°C) than water (100°C). Decreasing the temperature to condense the ethanol would also condense the water, so moles of gas from each side of the reaction are removed. The direction of equilibrium (yield) is unaffected when there is no net change in the number of moles of gas.

17.85 
$$n/V = M = P/RT = \frac{(2.0 \text{ atm})}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left((273.2 + 25.0) \text{K}\right)} = 0.0816919 M \text{ each gas}$$

$$\begin{array}{r} H_2(g) + \text{CO}_2(g) \leftrightarrows H_2O(g) + \text{CO}(g) \\ H_2(g) + 0.0816919 & 0 & 0 \\ \hline \text{Change} & -x & -x & +x & +x \\ \hline \text{Equi:} & 0.0816919 - x & 0.0816919 - x & x & x \\ \hline \text{Equi:} & 0.0816919 - x & 0.0816919 - x & x & x \\ \hline K_c = \frac{\left[\text{H}_2\text{O}\right]\left[\text{CO}\right]}{\left[\text{H}_2\right]\left[\text{CO}_2\right]} = 0.534 = \frac{\left[x\right]\left[x\right]}{\left[0.0816919 - x\right]\left[0.0816919 - x\right]} = \frac{\left[x\right]^2}{\left[0.0816919 - x\right]^2} \\ (0.534)^{1/2} = 0.730753 = \frac{\left[x\right]}{\left[0.0816919 - x\right]} \end{array}$$

x = 0.03449 M

M of H<sub>2</sub> at equilibrium = 0.0816919 - x = 0.0816919 - 0.03449 = 0.0472019 mol/L

Mass (g) of H<sub>2</sub> = 
$$(1.00 \text{ L}) \left( \frac{0.0472019 \text{ mol}}{\text{L}} \right) \left( \frac{2.016 \text{ g}}{1 \text{ mol}} \right) = 0.095159 = 0.095 \text{ g H}_2$$

17.86 To get the two equations to sum to the desired equation, the first equation must be reversed and doubled. This will result in squaring the reciprocal of its  $K_c$  value. The other equation does not need to be changed. Adding the two equations means the new  $K_c$  value will be the product of the individual  $K_c$  values.

$$\begin{array}{rcl} & \frac{2\text{NO}(g)}{2} \leftrightarrows & \text{N}_2(g) + \text{O}_2(g) & K_1 = (K_c)^{-2} = 4.340 \text{x} 10^{18} = K_2 \\ & \frac{2\text{NO}_2(g) \leftrightarrows & 2\text{NO}(g) + \text{O}_2(g) & K_2 = K_c = 1.1 \text{x} 10^{-5} \\ & \text{Overall: } 2\text{NO}_2(g) \leftrightarrows & \text{N}_2(g) + 2\text{O}_2(g) & K_c \text{ (overall)} = K_1 K_2 = 4.774 \text{x} 10^{13} = \textbf{4.8x} \textbf{10}^{13} M \end{array}$$

17.87 <u>Plan:</u> Write the equilibrium expression. You are given a value of  $K_c$  but the amounts of reactants and product are given in units of pressure. Convert  $K_c$  to  $K_p$  and use the equilibrium pressures of SO<sub>3</sub> and O<sub>2</sub> to obtain the equilibrium pressure of SO<sub>2</sub>. For part b), set up a reaction table and solve for x. The equilibrium concentrations can then be used to find the  $K_c$  value at the higher temperature. The concentration of SO<sub>2</sub> is converted to pressure using the ideal gas law, PV = nRT.

## Solution:

# a) $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$

 $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 3 = –1 (two mol of product, SO<sub>3</sub>, and three mol of reactants, 2 SO<sub>2</sub> + O<sub>2</sub>)

$$K_{\rm p} = K_{\rm c} (RT)^{\Delta n} = K_{\rm c} (RT)^{-1} = (1.7 \times 10^8) [(0.0821 \text{ L} \cdot \text{atm/mol} \cdot \text{K})(600. \text{ K})]^{-1} = 3.451 \times 10^6$$
  

$$K_{\rm p} = \frac{P_{\rm SO_3}^2}{P_{\rm SO_2}^2 P_{\rm O_2}} = \frac{(300.)^2}{P_{\rm SO_2}^2 (100.)} = 3.451 \times 10^6$$
  

$$P_{\rm SO_2} = 0.016149 = 0.016 \text{ atm}$$

b) Create a reaction table that describes the reaction conditions. Since the volume is 1.0 L, the moles equals the molarity. Note the 2:1:2 mole ratio between  $SO_2:O_2:SO_3$ .

Concentration ( <i>M</i> )	$2SO_2(g)$	+	$O_2(g)$	ţ	$2SO_3(g)$	
Initial	0.0040		0.0028		0	
Change	-2x		$-\mathbf{X}$		+2x	(2:1:2 mole ratio)
Equilibrium	0.0040 - 2x		0.0028 -	х	2x = 0.0	020 (given)
x = 0.0010, the	erefore:					

 $[SO_2] = 0.0040 - 2x = 0.0040 - 2(0.0010) = 0.0020 M$  $[O_2] = 0.0028 - x = 0.0028 - 0.0010 = 0.0018 M$  $[SO_3] = 2(0.0010) = 0.0020 M$ Substitute equilibrium concentrations into the equilibrium expression and solve for  $K_c$ .

$$K_{\rm c} = \frac{\left[{\rm SO}_3\right]^2}{\left[{\rm SO}_2\right]^2 \left[{\rm O}_2\right]} = \frac{\left[0.0020\right]^2}{\left[0.0020\right]^2 \left[0.0018\right]} = 555.5556 = 5.6 \text{x} 10^2$$

The pressure of  $SO_2$  is estimated using the concentration of  $SO_2$  and the ideal gas law (although the ideal gas law is not well behaved at high pressures and temperatures).

PV = nRT

$$P_{\rm SO_2} = \frac{nRT}{V} = \frac{(0.0020 \text{ mol})\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right)(1000. \text{ K})}{(1.0 \text{ L})} = 0.1642 = 0.16 \text{ atm}$$

17.88 The original concentrations are: (0.350 mol/0.500 L) = 0.700 M for CO and Cl<sub>2</sub>. Concentration (*M*) CO(g) + $Cl_2(g)$ ⇆  $COCl_2(g)$ 0.700 0.700 Initial 0 Change -x0.700 - x - x 0.700 - x +xEquilibrium  $Q_{c} = \frac{[\text{COCl}_{2}]}{[\text{CO}][\text{Cl}_{2}]} = \frac{[\text{x}]}{[0.700 - \text{x}][0.700 - \text{x}]} = \frac{[\text{x}]}{[0.490 - 1.400\text{x} + \text{x}^{2}]} = 4.95$  $4.95x^2 - 7.93x + 2.4255 = 0$ b = -7.93 c = 2.4255a = 4.95  $x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$  $x = \frac{-(-7.93) \pm \sqrt{(-7.93)^2 - 4(4.95)(2.4255)}}{2(4.95)}$ x = 1.19039 or 0.41162959

(The 1.19039 value is not possible because 0.700 - x would be negative.) [CO] = [Cl<sub>2</sub>] = 0.700 - x = 0.700 - 0.41162959 = 0.28837041 = 0.288 M[COCl<sub>2</sub>] = x = 0.41162959 = 0.412 M

17.89 <u>Plan:</u> Set up a reaction table to find the equilibrium amount of  $CaCO_3$  after the first equilibrium is established and then the equilibrium amount after the second equilibrium is established. Solution:

The equilibrium pressure of  $CO_2 = P_{CO_2} = 0.220$  atm.

Initial	$CaCO_3(s)$ 0.100 mol	) 5	CaO( <i>s</i> ) - 0.100 mol	+ C	$O_2(g)$
Change	- X		- X	+2	X
Equilibrium	0.100 - x		0.100 - x	2	$\overline{\mathbf{x}} = 0.220 \text{ atm (given)}$
				<b>C1</b>	

The amount of calcium carbonate solid in the container at the first equilibrium equals the original amount, 0.100 mol, minus the amount reacted to form 0.220 atm of carbon dioxide. The moles of  $CaCO_3$  reacted is equal to the number of moles of carbon dioxide produced. Use the pressure of  $CO_2$  and the ideal gas equation to calculate the moles of  $CO_2$  produced:

$$PV = nRT$$
  
Moles of CO<sub>2</sub> =  $n = \frac{PV}{RT}$   
 $n = \frac{(0.220 \text{ atm})(10.0 \text{ L})}{(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}})(385 \text{ K})} = 0.0696015 \text{ mol CO}_2$ 

Moles of  $CaCO_3$  reacted = moles of  $CO_2$  produced = 0.0696015 mol

Moles of  $CaCO_3$  remaining = initial moles - moles reacted = 0.100 mol  $CaCO_3 - 0.0696015$  mol  $CaCO_3$ = 0.0304 mol  $CaCO_3$  at first equilibrium

As more carbon dioxide gas is added, the system returns to equilibrium by shifting to the left to convert the added carbon dioxide to calcium carbonate to maintain the partial pressure of carbon dioxide at 0.220 atm ( $K_p$ ). Convert the added 0.300 atm of CO<sub>2</sub> to moles using the ideal gas equation. The moles of CO<sub>2</sub> reacted equals the moles of CaCO<sub>3</sub> formed.

Moles of CO<sub>2</sub> = 
$$n = \frac{PV}{RT}$$
  
 $n = \frac{(0.300 \text{ atm})(10.0 \text{ L})}{(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}})} = 0.09491 \text{ mol CO}_2$ 

Moles of  $CaCO_3$  produced = moles of  $CO_2$  reacted = 0.09491 mol  $CaCO_3$ Add the moles of  $CaCO_3$  formed in the second equilibrium to the moles of  $CaCO_3$  at the first equilibrium position.

Moles of  $CaCO_3$  = moles at first equilibrium + moles formed in second equilibrium = 0.0304 mol + 0.09491 = 0.12531mol CaCO\_3

Mass (g) of CaCO<sub>3</sub> = 
$$(0.12531 \text{ mol CaCO}_3) \left( \frac{100.09 \text{ g CaCO}_3}{1 \text{ mol CaCO}_3} \right) = 12.542 = 12.5 \text{ g CaCO}_3$$

17.90 a) 
$$C_2H_4(g) + 3O_2(g) \leftrightarrows 2CO_2(g) + 2H_2O(g)$$
  
b)  $4NO_2(g) + 6H_2O(g) \leftrightarrows 4NH_3(g) + 7O_2(g)$ 

17.91 
$$C_{2}H_{2}(g) + H_{2}(g) \leftrightarrows C_{2}H_{4}(g)$$
  

$$\Delta H_{rxn}^{\circ} = \Sigma m \Delta H_{products}^{\circ} - \Sigma n \Delta H_{reactants}^{\circ}$$

$$= \{1 \Delta H_{f}^{\circ} [C_{2}H_{4}(g)]\} - \{1 \Delta H_{f}^{\circ} [C_{2}H_{2}(g)] + 1 \Delta H_{f}^{\circ} [H_{2}(g)]\}$$

$$= [(1 \text{ mol})(52.47 \text{ kJ/mol})] - [(1 \text{ mol})(227 \text{ kJ/mol}) + (1 \text{ mol})(0.0 \text{ kJ/mol})]$$

$$= -174.53 \text{ kJ}$$

$$\ln \frac{K_{300}}{K_{2000}} = -\frac{\Delta H_{rxn}^{\circ}}{R} \left(\frac{1}{T_{2}} - \frac{1}{T_{1}}\right)$$

$$\ln \frac{K_{300}}{2.9 \text{x10}^{8}} = -\frac{(-174.53 \text{ kJ/mol})}{\left(8.314 \frac{\text{J}}{\text{mol} \cdot \text{K}}\right)} \left(\frac{1}{300. \text{ K}} - \frac{1}{2000. \text{ K}}\right) \left(\frac{10^{3} \text{ J}}{1 \text{ kJ}}\right)$$

$$\ln \frac{K_{300}}{2.9 \text{x10}^{8}} = 59.478189$$

$$\frac{K_{300}}{2.9 \text{x10}^{8}} = 6.77719 \text{x10}^{25}$$

$$K_{300} = (2.9 \text{x10}^{8})(6.77719 \text{x10}^{25}) = 1.9654 \text{x10}^{34} = 2.0 \text{x10}^{34}$$
17.92  $M_{2}(g) + N_{2}(g) \rightleftharpoons 2MN(g)$ 

$$K_{c} = \frac{[MN]^{2}}{[M_{2}][N_{2}]}$$
Scene A: Concentrations:  $[M_{2}] = [N_{2}] = 0.20 M$ ;  $[MN] = 0.40 M$ 

$$K_{c} = \frac{[0.40]^{2}}{[0.20][0.20]} = 4.0$$
  
Scene B:  
Concentration (M) M<sub>2</sub>(g) + N<sub>2</sub>(g) \(\Sigma\) 2MN(g)  
Initial 0.60 0.30 0

$$\frac{\text{Change} - x - x + 2x}{\text{Equilibrium} 0.60 - x 0.30 - x} 2x$$

$$K_{c} = 4.0 = \frac{\left[2x\right]^{2}}{\left[0.60 - x\right]\left[0.30 - x\right]}$$

$$4.0 = \frac{4x^{2}}{0.18 - 0.90 x + x^{2}}$$

$$4x^{2} = 0.72 - 3.6x + 4x^{2}$$

$$3.6x = 0.72$$

$$x = 0.20 M$$

$$[M_{2}] = 0.60 - x = 0.60 - 0.20 = 0.40 M$$

$$[M_{2}] = 0.30 - x = 0.30 - 0.20 = 0.10 M$$

$$[MN] = 2x = 2(0.20 M) = 0.40 M$$

17.93 <u>Plan:</u> Use the balanced reaction to write the equilibrium expression. The equilibrium concentration of  $S_2F_{10}$  is used to write an expression for the equilibrium concentrations of  $SF_4$  and  $SF_6$ . <u>Solution:</u>

 $\overline{\mathbf{S}_2\mathbf{F}_{10}(g)} \leftrightarrows \mathbf{SF}_4(g) + \mathbf{SF}_6(g)$ 

The reaction is described by the following equilibrium expression:

$$K_{\rm c} = \frac{\left[\mathrm{SF}_4\right]\left[\mathrm{SF}_6\right]}{\left[\mathrm{S}_2\mathrm{F}_{10}\right]}$$

At the first equilibrium,  $[S_2F_{10}] = 0.50 M$  and  $[SF_4] = [SF_6] = x ([SF_4]:[SF_6] = 1:1)$ .

$$K_{\rm c} = \frac{\left[\mathrm{SF}_{4}\right]\left[\mathrm{SF}_{6}\right]}{\left[\mathrm{S}_{2}\mathrm{F}_{10}\right]} = \frac{\left[\mathrm{x}\right]\left[\mathrm{x}\right]}{\left[0.50\right]}$$
$$\mathrm{x}^{2} = 0.50K_{\rm c}$$

$$[SF_4] = [SF_6] = x = \sqrt{0.50K_c}$$

At the second equilibrium,  $[S_2F_{10}] = 2.5 M$  and  $[SF_4] = [SF_6] = x$ .

$$K_{c} = \frac{[SF_{4}][SF_{6}]}{[S_{2}F_{10}]} = \frac{[x][x]}{[2.5]}$$
$$x^{2} = 2.5K_{c}$$
$$[SF_{4}] = [SF_{6}] = x = \sqrt{2.5K_{c}}$$

Thus, the concentrations of  $\mathrm{SF}_4$  and  $\mathrm{SF}_6$  increase by a factor of:

$$\frac{\sqrt{2.5K_c}}{\sqrt{0.50K_c}} = \frac{\sqrt{2.5}}{\sqrt{0.50}} = 2.236 = 2.2$$

17.94 Calculate  $K_c$ .

$$K_{\rm c} = \frac{[\rm CO_2][\rm H_2]}{[\rm CO][\rm H_2O]} = \frac{[0.40][0.10]}{[0.10][0.10]} = 4.0$$

Calculate new concentrations.

New H<sub>2</sub> = 0.10 *M* + (0.60 mol/2.0 L) = 0.40 *M*  
Concentration (*M*) CO(*g*) + H<sub>2</sub>O(*g*) 
$$\leftrightarrows$$
 CO<sub>2</sub>(*g*) + H<sub>2</sub>(*g*)  
Initial 0.10 0.10 0.40 0.40  
Change +x +x -x -x -x  
Equilibrium 0.10 + x 0.10 + x 0.40 - x 0.40 - x  
 $K_c = \frac{[CO_2][H_2]}{[CO][H_2O]} = \frac{[0.40 - x][0.40 - x]}{[0.10 + x][0.10 + x]} = \frac{[0.40 - x]^2}{[0.10 + x]^2} = 4.0$ 

$$\frac{\begin{bmatrix} 0.40 - x \end{bmatrix}}{\begin{bmatrix} 0.10 + x \end{bmatrix}} = 2.0$$
  
x = 0.066667  
[CO] = [H<sub>2</sub>O] = 0.10 + x = 0.10 + 0.066667 = 0.166667 = **0.17** *M*  
[CO<sub>2</sub>] = [H<sub>2</sub>] = 0.40 - x = 0.40 - 0.066667 = 0.333333 = **0.33** *M*

17.95 <u>Plan</u>: Use the volume fraction of  $O_2$  and  $CO_2$  to find the partial pressure of each gas and substitute these pressures into the equilibrium expression to find the partial pressure of CO. Use PV = nRT to convert the partial pressure of CO to moles per liter and then convert to pg/L. <u>Solution</u>:

a) Calculate the partial pressures of oxygen and carbon dioxide because volumes are proportional to moles of gas, so volume fraction equals mole fraction. Assume that the amount of carbon monoxide gas is small relative to the other gases, so the total volume of gases equals  $V_{CO_2} + V_{O_2} + V_{N_2} = 10.0 + 1.00 + 50.0 = 61.0$ .

$$P_{\text{CO}_2} = \left(\frac{10.0 \text{ mol CO}_2}{61.0 \text{ mol gas}}\right) (4.0 \text{ atm}) = 0.6557377 \text{ atm}$$
$$P_{\text{O}_2} = \left(\frac{1.00 \text{ mol O}_2}{61.0 \text{ mol gas}}\right) (4.0 \text{ atm}) = 0.06557377 \text{ atm}$$

Use the partial pressures and given  $K_p$  to find  $P_{CO}$ .

$$K_{\rm p} = \frac{P_{\rm CO}^2 P_{\rm O_2}}{P_{\rm CO_2}^2} = \frac{P_{\rm CO}^2 \left(0.06557377\right)}{\left(0.6557377\right)^2} = 1.4 \times 10^{-28}$$
$$P_{\rm CO} = 3.0299 \times 10^{-14} = 3.0 \times 10^{-14} \text{ atm}$$

b) 
$$PV = nRT$$
  

$$\frac{n_{CO}}{V} = \frac{P}{RT} = \frac{\left(3.0299 \times 10^{-14} \text{ atm}\right)}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) (800 \text{ K})} = 4.61312 \times 10^{-16} \text{ mol/L}$$
Concentration (pg/L) of CO =  $\left(\frac{4.61312 \times 10^{-16} \text{ mol CO}}{\text{L}}\right) \left(\frac{28.01 \text{ g CO}}{1 \text{ mol CO}}\right) \left(\frac{1 \text{ pg}}{10^{-12} \text{ g}}\right) = 0.01292 = 0.013 \text{ pg CO/L}$ 

- 17.96 Although the yield is favored by low temperature, the rate of formation is not. In fact, ammonia forms so slowly at low temperatures that the process becomes uneconomical. In practice, a compromise is achieved that optimizes yield and rate (high pressure, continual removal of NH<sub>3</sub>, increasing the temperature).
- 17.97 <u>Plan:</u> Write a reaction table given that  $P_{CH_4}$  (init) =  $P_{CO_2}$  (init) = 10.0 atm, substitute equilibrium values into the equilibrium expression, and solve for  $P_{H_2}$ .

Solution:  
a) Pressure (atm) 
$$CH_4(g) + CO_2(g) \rightleftharpoons 2CO(g) + 2H_2(g)$$
  
Initial 10.0 10.0 0 0  
Change  $-x$   $-x$   $+2x$   $+2x$   
Equilibrium  $10.0 - x$   $10.0 - x$   $2x$   $2x$   
 $K_p = \frac{P_{CO}^2 P_{H_2}^2}{P_{CH_4} P_{CO_2}} = \frac{(2x)^2 (2x)^2}{(10.0 - x)(10.0 - x)} = \frac{(2x)^4}{(10.0 - x)^2} = 3.548 \times 10^6$  (take square root of each side)  
 $\frac{(2x)^2}{(10.0 - x)} = 1.8836135 \times 10^3$   
A quadratic is necessary:  
 $4x^2 + (1.8836135 \times 10^3 x) - 1.8836135 \times 10^4 = 0$ 

$$a = 4 \quad b = 1.8836135 \times 10^{3} \quad c = -1.8836135 \times 10^{4}$$

$$x = \frac{-b \pm \sqrt{b^{2} - 4ac}}{2a}$$

$$x = \frac{-1.8836135 \times 10^{3} \pm \sqrt{\left(1.8836135 \times 10^{3}\right)^{2} - 4\left(4\right)\left(-1.8836135 \times 10^{4}\right)}}{2(4)}$$

$$x = 9.796209$$

 $P_{\rm H_2} = 2x = 2(9.796209) = 19.592419$  atm

If the reaction proceeded entirely to completion, the partial pressure of  $H_2$  would be 20.0 atm (pressure is proportional to moles, and twice as many moles of  $H_2$  form for each mole of  $CH_4$  or  $CO_2$  that reacts).

The percent yield is 
$$\frac{19.592418 \text{ atm}}{20.0 \text{ atm}} (100\%) = 97.96209 = 98.0\%.$$

b) Repeat the calculations for part a) with the new  $K_p$  value. The reaction table is the same.

$$K_{\rm p} = \frac{P_{\rm C0}^2 P_{\rm H_2}^2}{P_{\rm CH_4} P_{\rm CO_2}} = \frac{(2x)^2 (2x)^2}{(10.0 - x)(10.0 - x)} = \frac{(2x)^4}{(10.0 - x)^2} = 2.626 \times 10^7$$

$$\frac{(2x)^2}{(10.0 - x)} = 5.124451 \times 10^3$$
A quadratic is needed:
$$4x^2 + (5.124451 \times 10^3 x) - 5.124451 \times 10^4 = 0$$

$$a = 4 \qquad b = 5.124451 \times 10^3 \ c = -5.124451 \times 10^4$$

$$x = \frac{-5.124451 \times 10^3 \pm \sqrt{(5.124451 \times 10^3)^2 - 4(4)(-5.124451 \times 10^4)}}{2(4)}$$

$$x = 0.023144$$

$$x = 9.923144$$
  
 $P_{H_2} = 2x = 2(9.923144) = 19.84629$  atm

If the reaction proceeded entirely to completion, the partial pressure of  $H_2$  would be 20.0 atm (pressure is proportional to moles, and twice as many moles of  $H_2$  form for each mole of  $CH_4$  or  $CO_2$  that reacts).

The percent yield is 
$$\frac{19.84629 \text{ atm}}{20.0 \text{ atm}} (100\%) = 99.23145 = 99.0\%.$$

c) van't Hoff equation:

$$K_{1} = 3.548 \times 10^{6} \qquad T_{1} = 1200. \text{ K} \qquad \Delta H_{\text{rxn}}^{\circ} = ?$$

$$K_{2} = 2.626 \times 10^{7} \qquad T_{2} = 1300. \text{ K} \qquad R = 8.314 \text{ J/mol} \cdot \text{K}$$

$$\ln \frac{K_{2}}{K_{1}} = -\frac{\Delta H_{\text{rxn}}^{\circ}}{R} \left(\frac{1}{T_{2}} - \frac{1}{T_{1}}\right)$$

$$\ln \frac{2.626 \times 10^{7}}{3.548 \times 10^{6}} = -\frac{\Delta H_{\text{rxn}}^{\circ}}{\left(8.314 \frac{\text{J}}{\text{mol} \cdot \text{K}}\right)} \left(\frac{1}{1200. \text{ K}} - \frac{1}{1300. \text{ K}}\right)$$

 $2.0016628 = \Delta H_{\rm rxn}^{\circ} (7.710195 {\rm x} 10^{-6})$ 

 $\Delta H_{rxn}^{\circ} = 2.0016628/7.710195 \times 10^{-6} = 2.5961247 \times 10^{5} = 2.60 \times 10^{5} \text{ J/mol}$  (The subtraction of the 1/*T* terms limits the answer to three significant figures.)

17.98 a) 
$$\begin{array}{c} C_{3}H_{8}(g) + 3H_{2}O(g) \leftrightarrows 3CO(g) + 7H_{2}(g) \\ \hline 3CO(g) + 3H_{2}O(g) \leftrightarrows 3CO_{2}(g) + 3H_{2}(g) \\ \hline (Overall]: C_{3}H_{8}(g) + 6H_{2}O(g) \leftrightarrows 3CO_{2}(g) + 10H_{2}(g) \\ \hline b) K_{p(overall)} = K'_{p_{1}} \ge K'_{p_{2}} = (8.175 \pm 10^{15})(0.33483368) = 2.737265 \pm 10^{15} = 2.737 \pm 10^{15} \end{array}$$

c)  $K_{\rm p} = \frac{\left(P_{\rm CO_2}\right)^3 \left(P_{\rm H_2}\right)^{10}}{\left(P_{\rm C_3H_8}\right) \left(P_{\rm H_2O}\right)^6}$ 

The partial pressures of each reactant are proportional to the moles, and the limiting reactant may be determined from the partial pressures.

 $P_{C_{3}H_{8} \text{ (initial)}} = (1.00/5.00) \text{ x } 5.0 \text{ atm} = 1.0 \text{ atm}$  $P_{H_{2}O(\text{initial})} = (4.00/5.00) \text{ x } 5.0 \text{ atm} = 4.0 \text{ atm}$  (limiting reactant)

 $P_{\text{CO}_2(\text{formed})} = 4.0 \text{ atm } \text{H}_2\text{O} \text{ x} (3 \text{ mol } \text{CO}_2/6 \text{ mol } \text{H}_2\text{O}) = 2.0 \text{ atm}$ 

 $P_{\text{H}_2(\text{formed})} = 4.0 \text{ atm } \text{H}_2\text{O x} (10 \text{ mol } \text{H}_2/6 \text{ mol } \text{H}_2\text{O}) = 6.6667 \text{ atm}$ 

 $P_{C_{3}H_{8} (remaining)} = 1.0 \text{ atm } C_{3}H_{8} - [4.0 \text{ atm } H_{2}O \text{ x} (1 \text{ mol } C_{3}H_{8}/6 \text{ mol } H_{2}O)] = 0.3333 \text{ atm}$ 

 $P_{\rm H_2O(remaining)} = 0.00$  atm (limiting reactant)

 $P_{\text{Total}} = P_{\text{CO}_2} + P_{\text{H}_2} + P_{\text{C}_3\text{H}_8} + P_{\text{H}_2\text{O}} = 2.0 \text{ atm} + 6.6667 \text{ atm} + 0.3333 \text{ atm} + 0.00 \text{ atm} = 9.0 \text{ atm}$ d) Percent C<sub>3</sub>H<sub>8(unreacted)</sub> = [0.3333 \text{ atm}/1.0 \text{ atm}] x 100\% = 33.33\% = 30\%

17.99 <u>Plan</u>: Add the two reactions to obtain the overall reaction. Multiply the second equation by 2 to cancel the moles of CO produced in the first reaction.  $K_p$  for the second reaction is then  $(K_p)^2$ .  $K_p$  for the overall reaction is equal to the product of the  $K_p$  values for the two individual reactions. Calculate  $K_c$  using  $K_p = K_c (RT)^{\Delta n}$ . Solution:

$$2CH_4(g) + O_2(g) \leftrightarrows 2CO(g) + 4H_2(g) \qquad K_p = 9.34 \times 10^{28}$$
  
$$2CO(g) + 2H_2O(g) \leftrightarrows 2CO_2(g) + 2H_2(g) \qquad K_p = (1.374)^2 = 1.888$$

 $2CH_4(g) + O_2(g) + 2H_2O(g) \leftrightarrows 2CO_2(g) + 6H_2(g)$ b)  $K_p = (9.34 \times 10^{28})(1.888) = 1.76339 \times 10^{29} = 1.76 \times 10^{29}$ c)  $\Delta n$  = moles gaseous products – moles gaseous reactants = 8 - 5 = 3(8 moles of product gas – 5 moles of reactant gas)  $K_p = K_n (RT)^{\Delta n}$ 

$$K_{\rm c} = \frac{K_{\rm p}}{(RT)^{\Delta n}} = \frac{1.76339 \times 10^{29}}{\left[(0.0821 \text{ atm} \cdot \text{L/mol} \cdot \text{K})(1000)\right]^3} = 3.18654 \times 10^{23} = 3.19 \times 10^{23}$$

d) The initial total pressure is given as 30. atm. To find the final pressure use the relationship between pressure and number of moles of gas:  $n_{\text{initial}}/P_{\text{initial}} = n_{\text{final}}/P_{\text{final}}$ Total mol of gas initial = 2.0 mol CH<sub>4</sub> + 1.0 mol O<sub>2</sub> + 2.0 mol H<sub>2</sub>O = 5.0 mol

Total mol of gas final =  $2.0 \text{ mol } \text{CO}_2 + 6.0 \text{ mol } \text{H}_2 = 8.0 \text{ mol}$  (from mole ratios)

$$P_{\text{final}} = (30. \text{ atm reactants}) \left(\frac{8 \text{ mol products}}{5 \text{ mol reactants}}\right) = 48 \text{ atm}$$

17.100 <u>Plan</u>: Write an equilibrium expression. Use the balanced equation to define x and set up a reaction table, substitute into the equilibrium expression, and solve for x, from which the pressure of N or H is calculated. Convert log  $K_p$  to  $K_p$ . Convert pressures to moles using the ideal gas law, PV = nRT. Convert moles to atoms using Avogadro's number.

Solution:

a)

a) The initial pressure of N<sub>2</sub> is 200. atm.  
Pressure (atm) N<sub>2</sub>(g) 
$$\rightleftharpoons$$
 2N(g)  
Initial 200. 0  
Change -x +2x  
Equilibrium  $200 - x - 2x$   
 $K_p = \frac{(P_N)^2}{(P_{N_2})} = 7.94328 \times 10^{-44}$   
 $\frac{(2x)^2}{(200. - x)} = 7.94328 \times 10^{-44}$  Assume  $200. - x \cong 200$ .

$$\begin{aligned} \left(\frac{2x}{(200)}\right)^2 &= 7.94328 \times 10^{-44} \\ &4x^2 &= 1.588656 \times 10^{-44} \\ &x &= 1.992897 \times 10^{-21} \\ P_N &= 2x &= 2(1.992897 \times 10^{-21}) \\ &= 3.985795 \times 10^{-21} = 4.0 \times 10^{-21} \text{ atm} \end{aligned} \\ b) \ \text{Log } K_p &= -17.30; \quad K_p &= 10^{-17.30} \\ &= 5.01187 \times 10^{-18} \\ &\text{Pressure (atm)} \quad H_2(g) &\cong 2H(g) \\ \text{Initial} & 600 & 0 \\ \hline \frac{\text{Change} &-x &+ 2x}{\text{Equilibrium}} \\ &= \frac{(P_H)^2}{(P_{H_2})} \\ &= 5.01187 \times 10^{-18} \\ &\frac{(2x)^2}{(600 - x)} \\ &= 5.01187 \times 10^{-18} \\ \hline \frac{(2x)^2}{(600)} \\ &= 5.01187 \times 10^{-18} \\ &4x^2 &= 3.007122 \times 10^{-15} \\ &x &= 2.741862 \times 10^{-8} \\ &= 5.48372 \times 10^{-8} \\ &= 5.5 \times 10^{-8} \end{aligned}$$
  

$$c) \ PV &= nRT \\ \text{Moles of N atoms} &= \frac{PV}{RT} \\ &= \frac{(3.985795 \times 10^{-21} \text{ atm})(1.00 \text{ L})}{(0.0821 \frac{1 \text{ ratm}}{\text{mol} \text{ K}})(1000 \text{ K})} \\ &= 4.85481 \times 10^{-15} \text{ mol} \\ \text{Mulber of N atoms} &= \frac{PV}{RT} \\ &= \frac{(5.48372 \times 10^{-8} \text{ atm})(1.00 \text{ L})}{(0.0821 \frac{1 \text{ ratm}}{\text{mol} \text{ mol} \text{ K}})(1000 \text{ K})} \\ &= 29.2356 = 29 \text{ N atoms/T} \\ \text{Moles of H atoms} &= \frac{PV}{RT} \\ &= \frac{(5.48372 \times 10^{-8} \text{ atm})(1.00 \text{ L})}{(0.0821 \frac{1 \text{ ratm}}{\text{mol} \text{ mol} \text{ K}})(1000 \text{ K})} \\ &= 4.022 \times 10^{-10} \text{ mol} \end{aligned}$$

d) The more reasonable step is  $N_2(g) + H(g) \rightarrow NH(g) + N(g)$ . With only twenty-nine N atoms in 1.0 L, the first reaction would produce virtually no NH(g) molecules. There are orders of magnitude more N<sub>2</sub> molecules than N atoms, so the second reaction is the more reasonable step.

17.101 a) Scenes B and D represent equilibrium. b) C, A, B = D c) [Y] =  $(4 \text{ spheres}) \left( \frac{0.025 \text{ mol}}{1 \text{ sphere}} \right) \left( \frac{1}{0.40 \text{ L}} \right) = 0.25 \text{ M}$ 

$$[\mathbf{Z}] = (8 \text{ spheres}) \left(\frac{0.025 \text{ mol}}{1 \text{ sphere}}\right) \left(\frac{1}{0.40 \text{ L}}\right) = 0.50 \text{ M}$$

$$K_{\rm c} = \frac{[Z]^2}{[Y]} = \frac{[0.50]^2}{[0.25]} = 1.0$$

17.102 The K is very small, thus the reaction will shift to the right to reach equilibrium. To simplify the calculations, assume the equilibrium shifts entirely to the left, and then a little material reacts to reach equilibrium. Shifting entirely to the left gives  $[H_2S] = 0.600$ , and  $[H_2] = [S_2] = 0$ .

$$\begin{array}{rcl} 2H_2S(g) &\leftrightarrows 2H_2(g) + S_2(g)\\ \text{Initial} & 0.600 \ M & 0 \ M & 0 \ M\\ \hline \frac{\text{Change} & -2x & +2x & +x}{\text{Equilibrium}} \\ & 0.600 - 2x & 2x & x \\ \hline \text{Equilibrium} & 0.600 - 2x & 2x & x \\ \hline K_c &= \frac{\left[H_2\right]^2 \left[S_2\right]}{\left[H_2S\right]^2} = 9.0x10^{-8} \\ & \frac{\left[2x\right]^2 \left[x\right]}{\left[0.600 - 2x\right]^2} = 9.0x10^{-8} \\ & \frac{\left[2x\right]^2 \left[x\right]}{\left[0.600\right]^2} = 9.0x10^{-8} \\ & x = 2.008x10^{-3} & (\text{assumption justified}) \\ \hline (H_2S) &= 0.600 - 2x = 0.600 - 2(2.008x10^{-3}) = 0.595984 = 0.596 \ M \ H_2S \\ \hline (H_2) &= 2x = 2(2.008x10^{-3}) = 4.016x10^{-3} = 4.0x10^{-3} \ M \ H_2 \\ \hline S_2 &= x = 2.008x10^{-3} = 2.0x10^{-3} \ M \ S_2 \end{array}$$

17.103 Plan: Write an equilibrium expression. Use the balanced equation to define x and set up a reaction table, substitute into the equilibrium expression, and solve for x, from which the equilibrium pressures of the gases are calculated. Add the equilibrium pressures of the three gases to obtain the total pressure. Use the relationship  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$  to find  $K_{\rm c}$ .

a)

Pressure (atm) 
$$N_2(g) + O_2(g) \leftrightarrows 2NO(g)$$
  
Initial 0.780 0.210 0  
Change -x -x +2x  
Equilibrium 0.780 - x 0.210 - x 2x  
 $K_p = \frac{(P_{NO})^2}{(P_{N_2})(P_{O_2})} = 4.35 \times 10^{-31}$   
 $\frac{(2x)^2}{(0.780 - x)(0.210 - x)} = 4.35 \times 10^{-31}$  Assume x is small because K is small  
 $\frac{(2x)^2}{(0.780)(0.210)} = 4.35 \times 10^{-31}$   
 $x = 1.33466 \times 10^{-16}$ 

Based on the small amount of nitrogen monoxide formed, the assumption that the partial pressures of nitrogen and oxygen change to an insignificant degree holds.

Oxygen change to an insignificant degree holds.  $P_{\text{nitrogen}}$  (equilibrium) = (0.780 - 1.33466x10<sup>-16</sup>) atm = **0.780 atm N<sub>2</sub>**   $P_{\text{oxygen}}$  (equilibrium) = (0.210 - 1.33466x10<sup>-16</sup>) atm = **0.210 atm O<sub>2</sub>**   $P_{\text{NO}}$  (equilibrium) = 2(1.33466x10<sup>-16</sup>) atm = 2.66933x10<sup>-16</sup> = **2.67x10<sup>-16</sup> atm NO** b) The total pressure is the sum of the three partial pressures: 0.780 atm + 0.210 atm + 2.67x10<sup>-16</sup> atm = **0.990 atm** c)  $K_{\text{p}} = K_{\text{c}}(RT)^{\Delta n}$ 

 $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 2 = 0 (two moles of product NO and two moles of reactants N<sub>2</sub> and O<sub>2</sub>)

 $K_p = K_c (RT)^0$  $K_c = K_p = 4.35 \times 10^{-31}$  because there is no net increase or decrease in the number of moles of gas in the course of the reaction.

17.104 a) 
$$K_{\rm p} = K_{\rm c} (RT)^{\Delta n} \ n = 2 - (2 + 1) = -1$$
  
 $K_{\rm c} = K_{\rm p} / (RT)^{\Delta n}$   
 $K_{\rm c} = \frac{\left(1.3 \times 10^4\right)}{\left[\left(0.0821\right)\left(457\right)\right]^{-1}} = 4.877561 \times 10^5 = 4.9 \times 10^5$ 

b) 
$$\Delta H_{rxn}^{\circ} = \sum [\Delta H_{f(products)}^{\circ}] - \sum [\Delta H_{f(reactants)}^{\circ}]$$
  
 $\Delta H_{rxn}^{\circ} = \{2 \Delta H_{f}^{\circ} [NO_{2}(g)]\} - \{2 \Delta H_{f}^{\circ} [NO(g)] + 1 \Delta H_{f}^{\circ} [O_{2}(g)]\}$   
 $= [(2 mol)(33.2 kJ/mol)] - [(2 mol)(90.29 kJ/mol) + (1 mol)(0.0 kJ/mol)]$   
 $= -114.18 = -114.2 kJ$   
c)  $\ln \frac{K_{2}}{K_{1}} = -\frac{\Delta H_{rxn}^{\circ}}{R} \left(\frac{1}{T_{2}} - \frac{1}{T_{1}}\right)$   
 $\ln \frac{6.4x10^{9}}{4.877561x10^{5}} = -\frac{-114.18 kJ}{8.314 J/mol \cdot K} \left(\frac{1}{T_{2}} - \frac{1}{457 K}\right) \left(\frac{10^{3} J}{1 kJ}\right)$   
9.4819931 = 13,733  $\left(\frac{1}{T_{2}} - \frac{1}{457 K}\right)$   
 $T_{2} = 347.389 = 3.5x10^{2} K$ 

17.105 <u>Plan</u>: Use the equation  $K_p = K_c (RT)^{\Delta n}$  to find  $K_p$ . The value of  $K_c$  for the formation of HI is the reciprocal of the  $K_{\rm c}$  value for the decomposition of HI. Use the equation  $\Delta H_{\rm rxn}^{\circ} = \sum [\Delta H_{\rm f(products)}^{\circ}] - \sum [\Delta H_{\rm f(reactants)}^{\circ}]$  to find the

value of  $\Delta H_{rxn}^{\circ}$ . Use the van't Hoff equation as a second method of calculating  $\Delta H_{rxn}^{\circ}$ .

Solution: a) $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$  $\Delta n$  = moles gaseous products – moles gaseous reactants = 2 – 2 = 0 (2 mol product  $(1H_2 + 1I_2) - 2$  mol reactant (HI) = 0)  $K_p = K_c (RT)^0 = 1.26 \times 10^{-3} (RT)^0 = 1.26 \times 10^{-3}$ b) The equilibrium constant for the reverse reaction is the reciprocal of the equilibrium constant for the

forward reaction:

$$K_{\text{formation}} = \frac{1}{K_{\text{decomposition}}} = \frac{1}{1.26 \times 10^{-3}} = 793.65 = 794$$

c) 
$$\Delta H_{rxn}^{\circ} = \sum [\Delta H_{f(products)}^{\circ}] - \sum [\Delta H_{f(reactants)}^{\circ}]$$
  
 $\Delta H_{rxn}^{\circ} = \{1 \Delta H_{f}^{\circ} [H_{2}(g)] + 1 \Delta H_{f}^{\circ} [I_{2}(g)]\} - \{2 \Delta H_{f}^{\circ} [HI(g)]\}$   
 $\Delta H_{rxn}^{\circ} = [(1 \text{ mol})(0 \text{ kJ/mol}) + (1 \text{ mol})(0 \text{ kJ/mol})] - [(2 \text{ mol})(25.9 \text{ kJ/mol})]$   
 $\Delta H_{rxn}^{\circ} = -51.8 \text{ kJ}$   
d)  $\ln \frac{K_{2}}{K_{1}} = -\frac{\Delta H_{rxn}^{\circ}}{R} \left(\frac{1}{T_{2}} - \frac{1}{T_{1}}\right)$   
 $K_{1} = 1.26 \times 10^{-3}; K_{2} = 2.0 \times 10^{-2}, T_{1} = 298 \text{ K}; T_{2} = 729 \text{ K}$   
 $\ln \frac{2.0 \times 10^{-2}}{1.26 \times 10^{-3}} = -\frac{\Delta H_{rxn}^{\circ}}{8.314 \text{ J/mol} \cdot \text{K}} \left(\frac{1}{729 \text{ K}} - \frac{1}{298 \text{ K}}\right)$ 

 $2.764621 = 2.38629 \times 10^{-4} \Delta H_{\rm rxn}^{\circ}$ 

 $\Delta H_{rxn}^{\circ} = 1.1585 x 10^4 = 1.2 x 10^4$  J/mol

17.106  $C_5H_{11}OH + CH_3COOH \leftrightarrows CH_3COOC_5H_{11} + H_2O$ Removing water should help to increase the yield of banana oil. Both isopentyl alcohol and acetic acid are more soluble in water than isopentyl acetate. Thus, removing water will increase the concentration of both reactants and cause a shift in equilibrium towards the products.

17.107 Q(g) 
$$\leftrightarrows$$
 R(g)  $K = \frac{[R]}{[Q]}$ 

For Scene A at equilibrium:

$$K = \frac{[R]}{[Q]} = \frac{[2]}{[6]} = 0.33$$

For Scene B:

FOI Scelle D.			
	Q(g)	⇆	$\mathbf{R}(g)$
Initial	10		2
Change	-X		+x
Equilibrium	10 - x		2 + x
$0.33 = \frac{[2+x]}{[10-x]}$			
x = 0.977 = 1			
Q = 10 - x = 10	- 1 = <b>9</b> ; <b>H</b>	R = 2 + 1	+ x = 2 + 1 = 3

17.108 a) 
$$K_{\rm p} = \left(P_{\rm H_2O}\right)^{10} = 4.08 \times 10^{-25}$$
  
 $P_{\rm H_2O} = \sqrt[10]{4.08 \times 10^{-25}} = 3.6397 \times 10^{-3} = 3.64 \times 10^{-3}$ 

b) (1) Adding more Na<sub>2</sub>SO<sub>4</sub>(s) will decrease the ratio of hydrated form/anhydrous form merely because you are increasing the value of the denominator, not because the equilibrium shifts.
(2) Reducing the container size will increase the pressure (concentration) of the water vapor, which will shift the equilibrium to the reactant side. The ratio of hydrated form/anhydrous form will increase.
(3) Adding more water vapor will increase the concentration of the water vapor, which will shift the equilibrium to the reactant side. The ratio of hydrated form/anhydrous form will increase.
(4) Adding N<sub>2</sub> gas will not change the partial pressure of the water vapor, so the ratio of hydrated form/anhydrous form will increase.

atm

17.109 <u>Plan:</u> Use the balanced equation to write an equilibrium expression. Find the initial concentration of each reactant from the given amounts and container volume, use the balanced equation to define x, and set up a reaction table. The equilibrium concentration of CO is known, so x can be calculated and used to find the other equilibrium concentrations. Substitute the equilibrium concentrations into the equilibrium expression to find  $K_c$ . Add the molarities of all of the gases at equilibrium, use (M)(V) to find the total number of moles, and then use PV = nRT to find the total pressure. To find [CO]<sub>eq</sub> after the pressure is doubled, set up another reaction table in which the initial concentrations are equal to the final concentrations from part a) and add in the additional CO. Solution:

The reaction is:  $CO(g) + H_2O(g) \leftrightarrows CO_2(g) + H_2(g)$ a) Initial [CO] and initial  $[H_2O] = 0.100 \text{ mol}/20.00 \text{ L} = 0.00500 \text{ M}.$ 

	CO	$H_2O$	与	$CO_2$	$H_2$
Initial	0.00500 M	0.00500 M	[	0	0
Change	X	X		+x	$+\mathbf{x}$
Equilibrium	0.00500 - x	0.00500 -	х	Х	Х
[CO] <sub>equilibrium</sub> =	= 0.00500 - x = 2.2	$24 \times 10^{-3} M = [1]$	$H_2O$ ]	(given in	problem)
$\mathbf{x} = 0$	$.00276 M = [CO_2]$	$= [H_2]$			

$$K_{c} = \frac{[CO_{2}][H_{2}]}{[CO][H_{2}O]} = \frac{[0.00276][0.00276]}{[0.00224][0.00224]} = 1.518176 = 1.52$$
  
b)  $M_{\text{total}} = [CO] + [H_{2}O] + [CO_{2}] + [H_{2}] = (0.00224 M) + (0.00224 M) + (0.00276 M) + (0.00276 M) + (0.00276 M) + (0.00276 M) = 0.01000 M$   
 $n_{\text{total}} = (M_{\text{total}})(V) = (0.01000 \text{ mol/L})(20.00 \text{ L}) = 0.2000 \text{ mol total}$   
 $PV = nRT$   
 $(0.2000 \text{ mol}) \Big( 0.08206 \frac{\text{L} \cdot \text{atm}}{1 + V} \Big) \Big( (273 + 900.) \text{ K} \Big)$ 

$$P_{\text{total}} = n_{\text{total}} RT/V = \frac{(0.2000 \text{ mol})(0.08206 \frac{\text{mol} \cdot \text{K}}{\text{mol} \cdot \text{K}})((273 + 900.) \text{ K})}{(20.00 \text{ L})} = 0.9625638 = 0.9626 \text{ atm}$$

c) Initially, an equal number of moles must be added = 0.2000 mol COd) Set up a table with the initial concentrations equal to the final concentrations from part a), and then add 0.2000 mol CO/20.00 L = 0.01000 M to compensate for the added CO.

Initial 0.00224 M 0.00224 M 0.00276 M 0.00276 M  
Added CO 0.01000 M  
Change -x -x +x +x +x  
Equilibrium 0.01224 - x 0.00224 - x 0.00276 + x 0.00276 + x  

$$K_{c} = \frac{\left[CO_{2}\right]\left[H_{2}\right]}{\left[CO\right]\left[H_{2}O\right]} = \frac{\left[0.00276 + x\right]\left[0.00276 + x\right]}{\left[0.01224 - x\right]\left[0.00224 - x\right]} = 1.518176$$

$$\frac{\left[7.6176x10^{-6} + 5.52x10^{-3}x + x^{2}\right]}{2.74176x10^{-5} - 1.448x10^{-2}x + x^{2}} = 1.518176$$

$$7.6176x10^{-6} + 5.52x10^{-3}x + x^{2} = (1.518176)(2.74176x10^{-5} - 1.448x10^{-2}x + x^{2})$$

$$7.6176x10^{-6} + 5.52x10^{-3}x + x^{2} = 4.162474x10^{-5} - 0.021983x + 1.518176x^{2}$$

$$0.518176x^{2} - 0.027503x + 3.400714x10^{-5} = 0$$

$$a = 0.518176 b = -0.027503 c = 3.400714x10^{-5}$$

$$x = \frac{-b \pm \sqrt{b^{2} - 4ac}}{2a}$$

$$x = \frac{-(-0.027503) \pm \sqrt{(-0.027503)^{2} - 4(0.518176)(3.400714x10^{-5})}}{2(0.518176)}$$

$$x = 1.31277x10^{-3}$$

$$[CO] = 0.01224 - x = 0.01224 - (1.31277x10^{-3}) = 0.01092723 = 0.01093 M$$

17.110 a) At point A the sign of Δ*H*° is negative for the reaction graphite → diamond. An increase in temperature at constant pressure will cause the formation of more graphite. Therefore, the equation must look like this: graphite → diamond + heat, and adding heat shifts the equilibrium to the reactant side.
b) Diamond is denser than graphite. The slope of the diamond-graphite line is positive. An increase in pressure favors the formation of diamond.